

Modelling Radar Biases Due to Antenna Topology and Operating Frequency

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ERAD 2018

10th European Conference on Radar in Meteorology & Hydrology
Ede, Netherlands
1-6 July 2018

Z_{DR}

1976 was A long, long time ago.....

- First Star Wars Movie!!
- Human Accomplishments since 1976:
 - Personal computer revolution
 - Human genome mapped
 - Cosmic string theory introduced (1976, Thomas Kibble)
 - Internet
 - GPS navigation
 - Cell phones

• But what can't we do well yet???

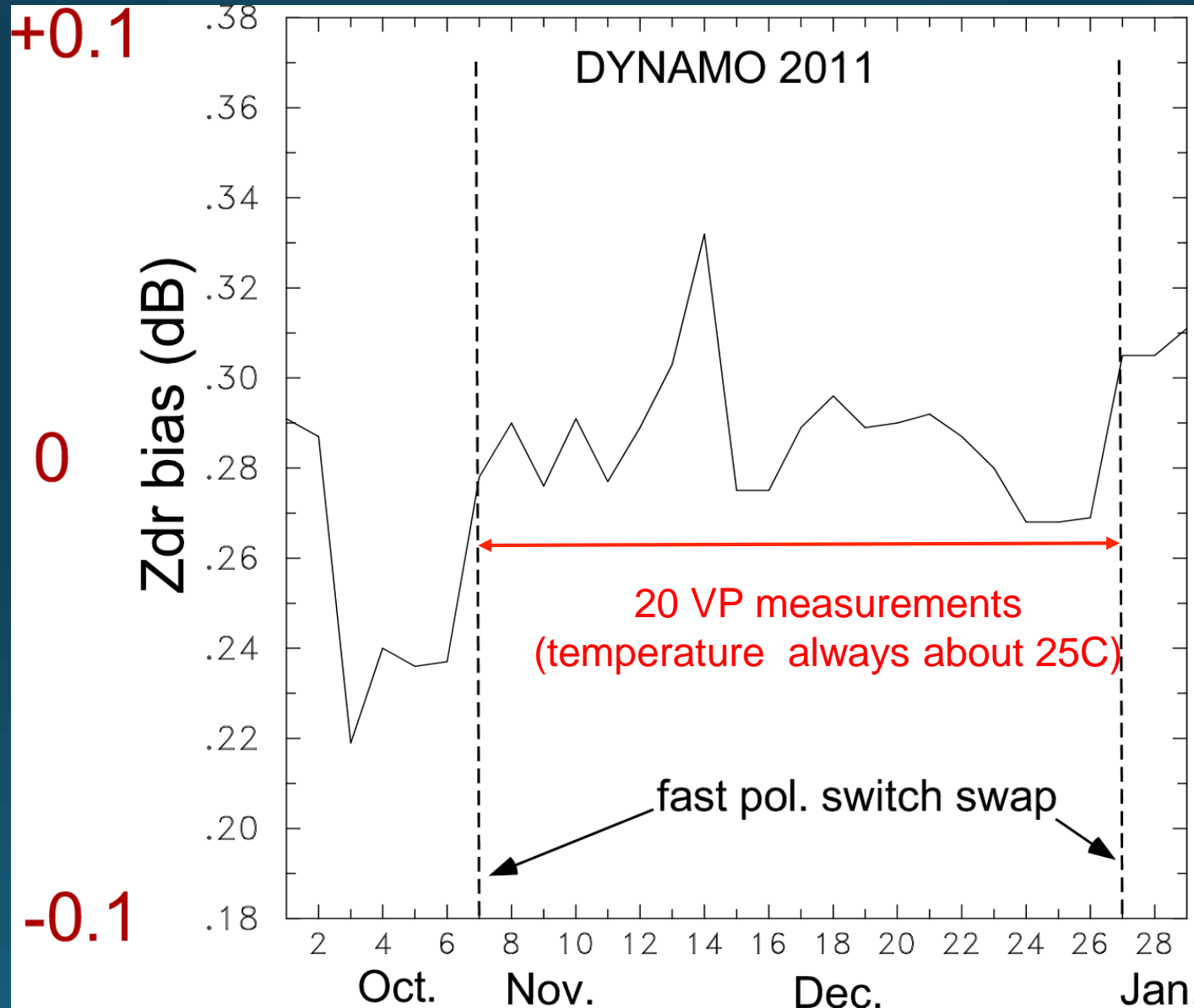
• Why is that Yoda??



S-Pol Zdr Calibration Story

Previous Zdr VP Cal Experience with S-Pol

Zdr bias very stable!!

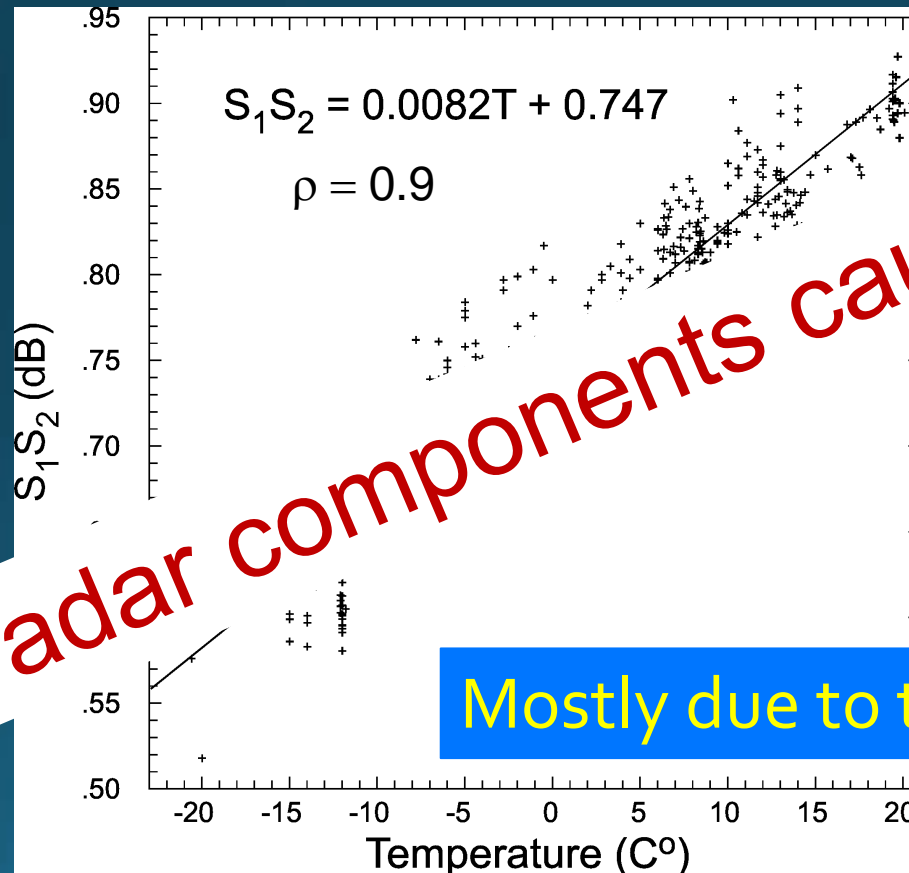


Zdr bias versus Air Temperature

MASCRAD Experiment: 104-2015 in Front Range

Data gathered in Colorado Front Range with S-Pol

December 24, 26, 2014 , January 9, 10, 11, 12, 15, and Feb. 6, 22, 27, 2015



What radar components cause this!!

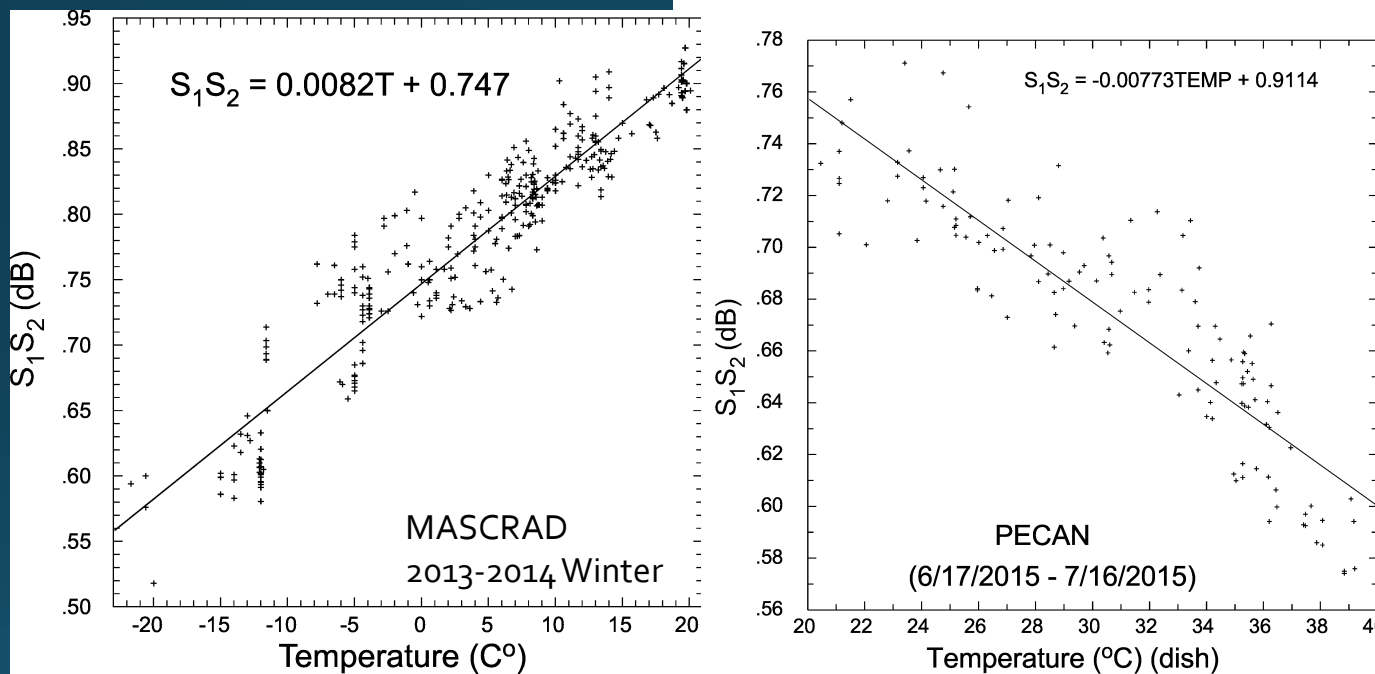
Mostly due to the antenna

MASCRAD and PECAN Experiments

S_1S_2 versus Temperature

RF diff. gain < 0.03dB

Temperature Ranges do not Overlap



Tear down/set up.
Microwave absorber on struts

BACKGROUND

Z_{dr} Calibration:

Crosspolar Power Technique

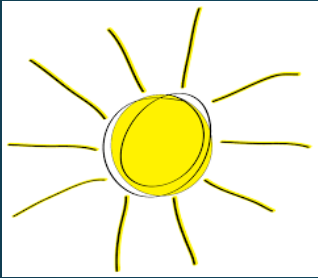
$$Z_{dr}^{cal} = Z_{dr}^m S_1 S_2 \frac{P_{xV}}{P_{xH}}$$

Solar power ratio

Crosspolar power ratio



Using the previous regression fit of $S_1 S_2$ to temperature, PECAN Z_{dr} was calibrated.

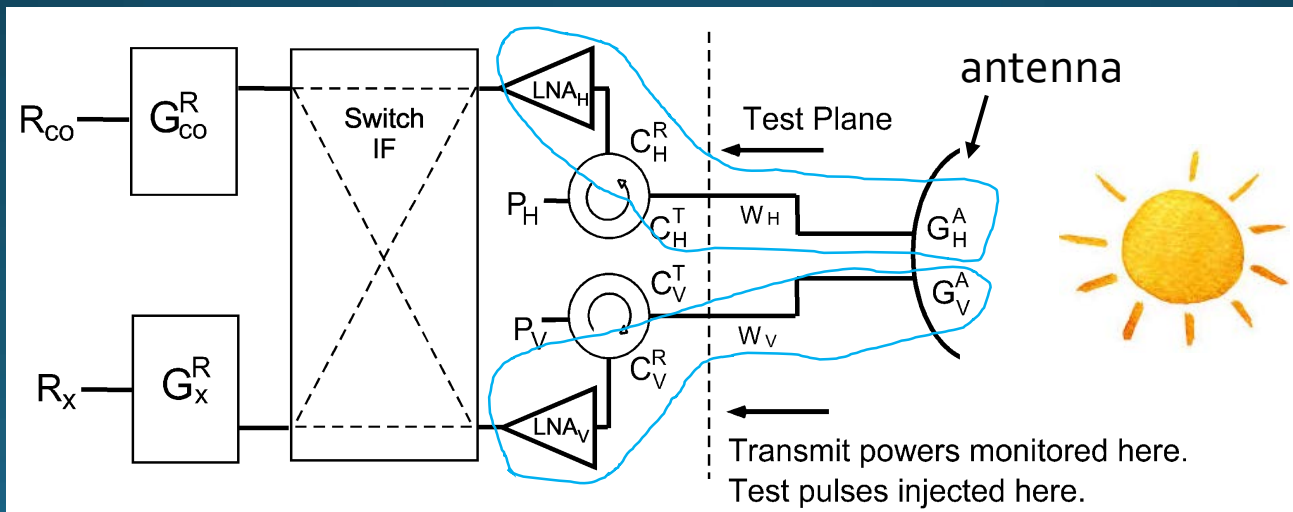


S₁S₂ Consists of Two Terms

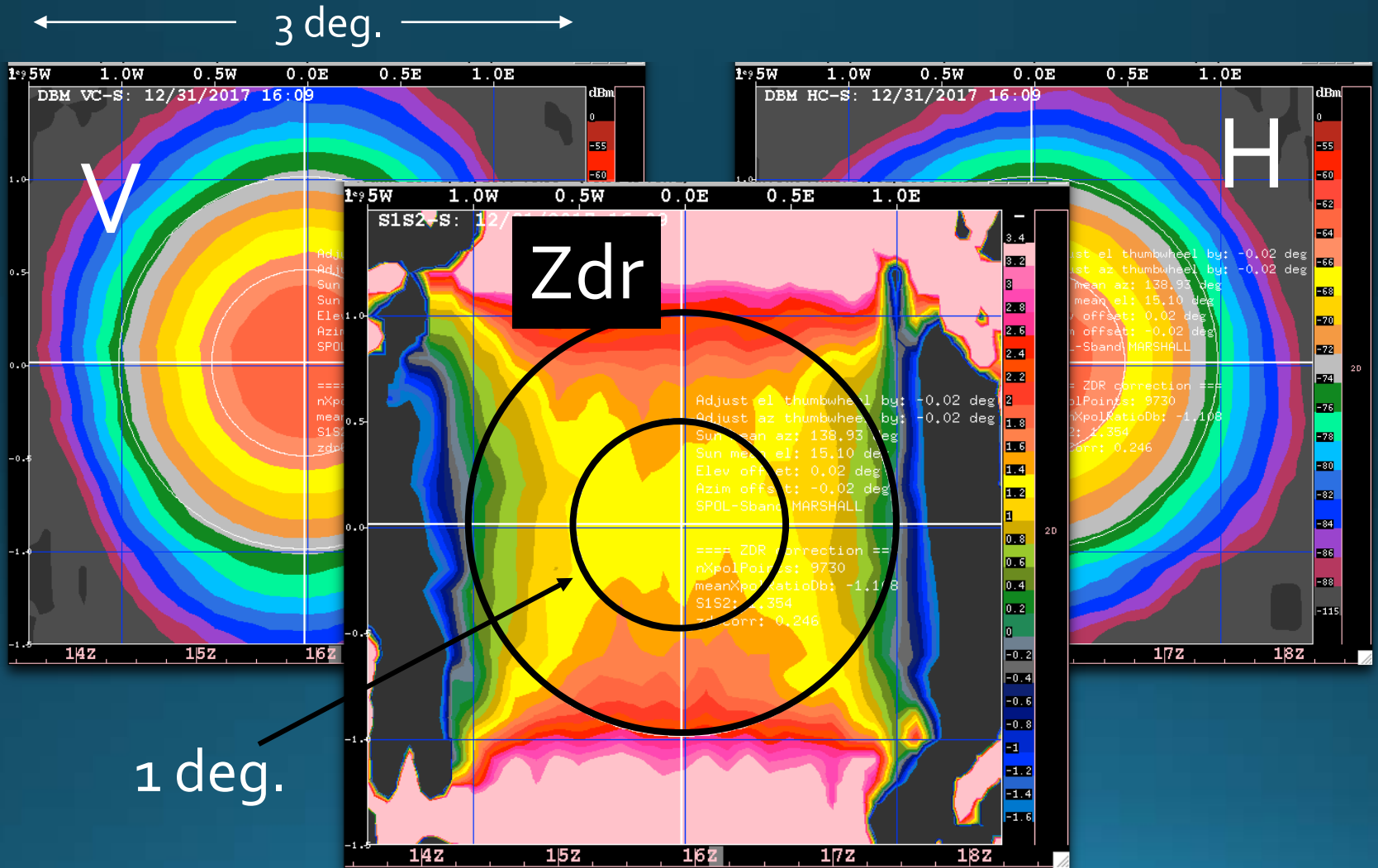
Antenna

RF Receiver

$$S_1 S_2 = \frac{(W_V G_V^A C_V^R LNA_V)^2}{(W_H G_H^A C_H^R LNA_H)^2}$$

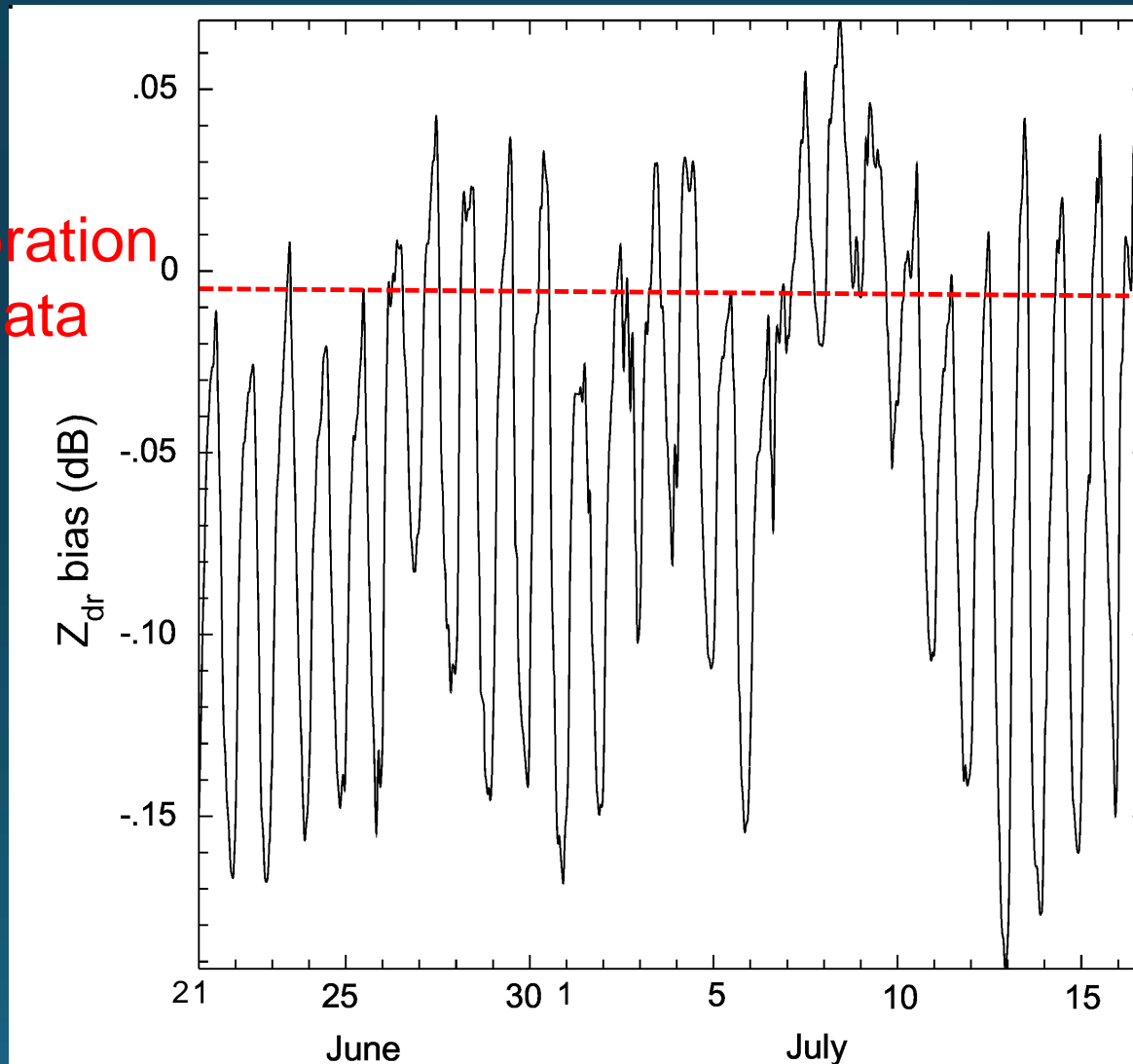


Experimental Solar Antenna Patterns



Zdr Bias Calibration for PECAN

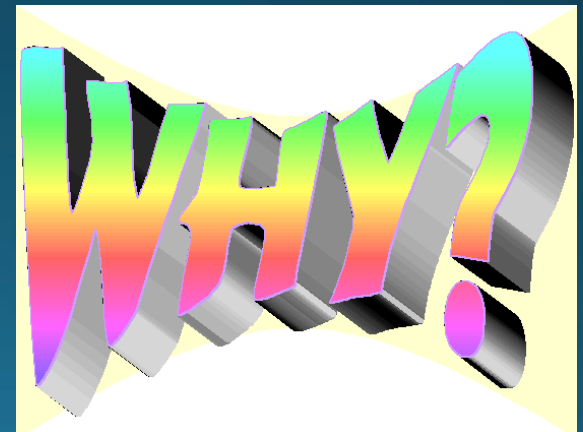
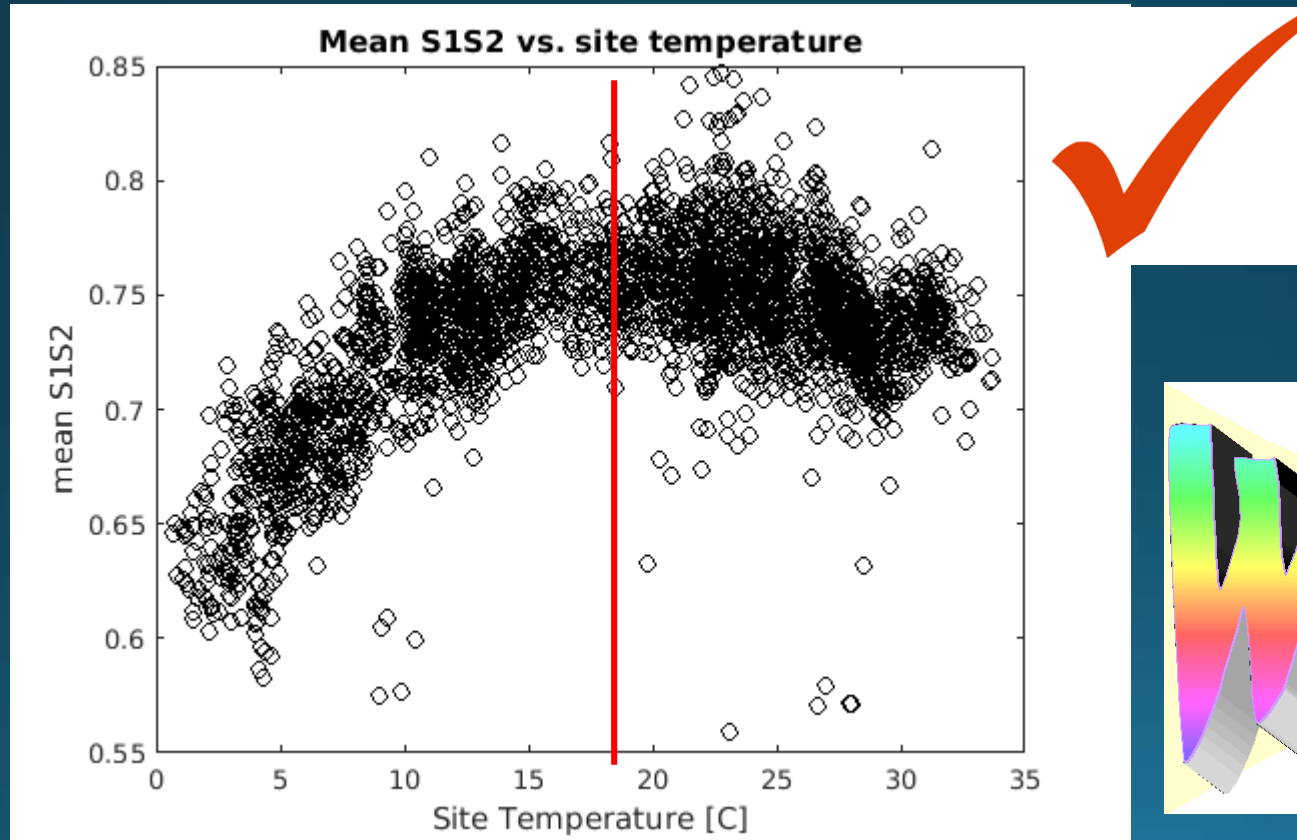
Legacy calibration
from VP data



S_1S_2 Measurement from this Spring

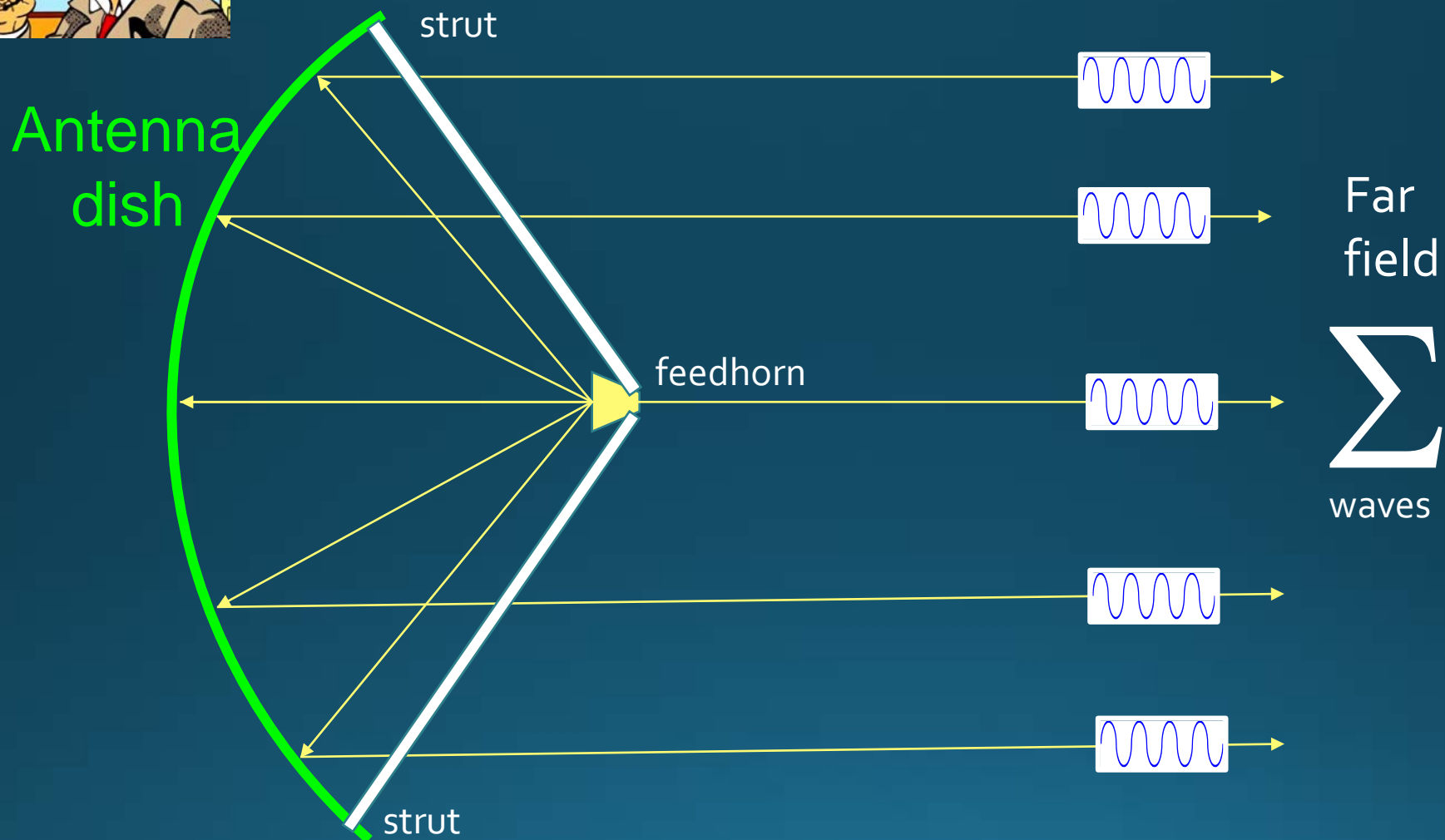
S-Pol at Marshall Fieldsite, April – June, 2017

Indeed there is an inflection point at 18 to 20C!!





Likely Mechanism for Zdr Bias Variations

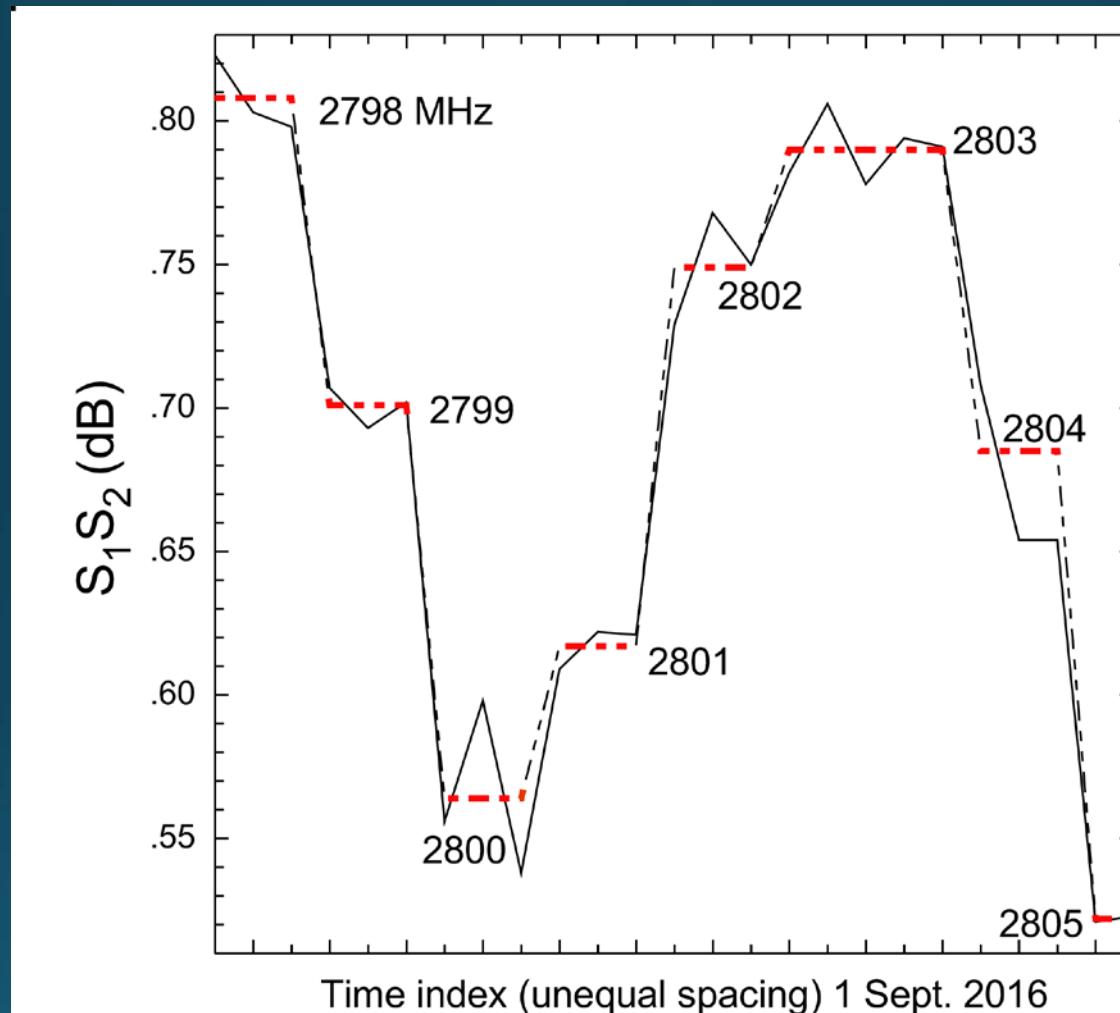


As metal expands , Phase relationships change

Idea

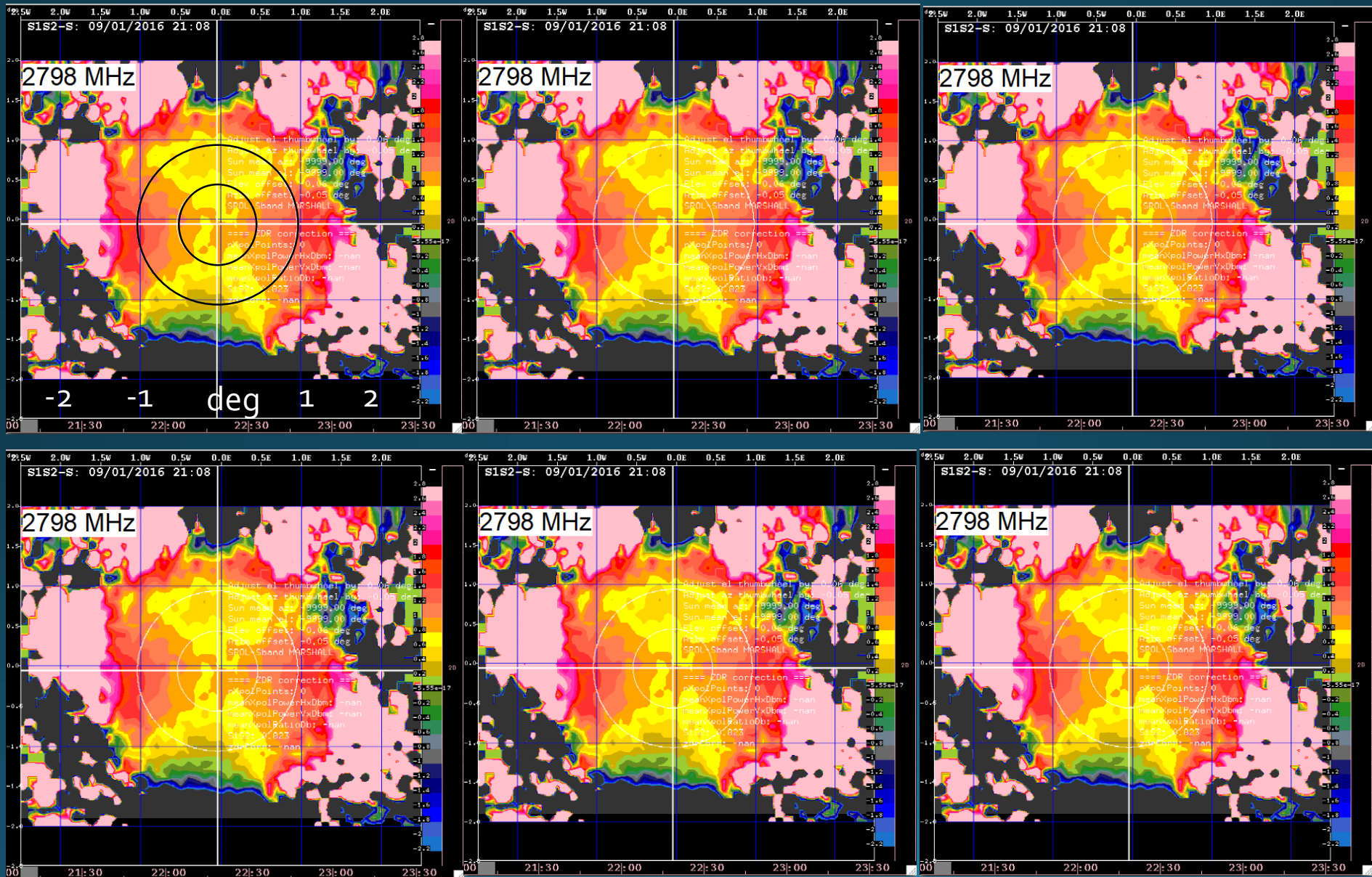
- Change phase relationships by changing frequency

$S_1 S_2$ as a Function of Frequency

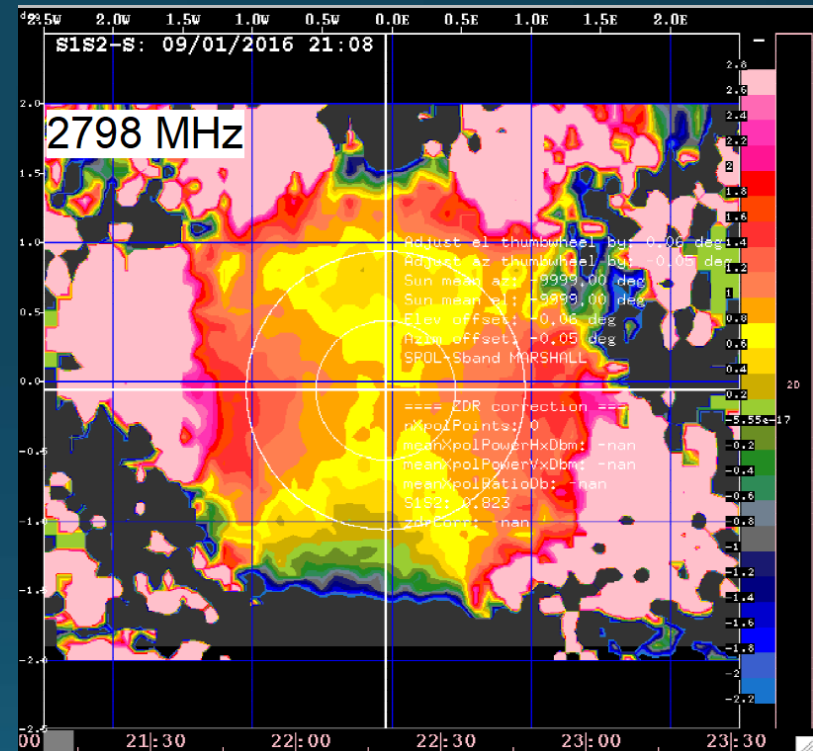
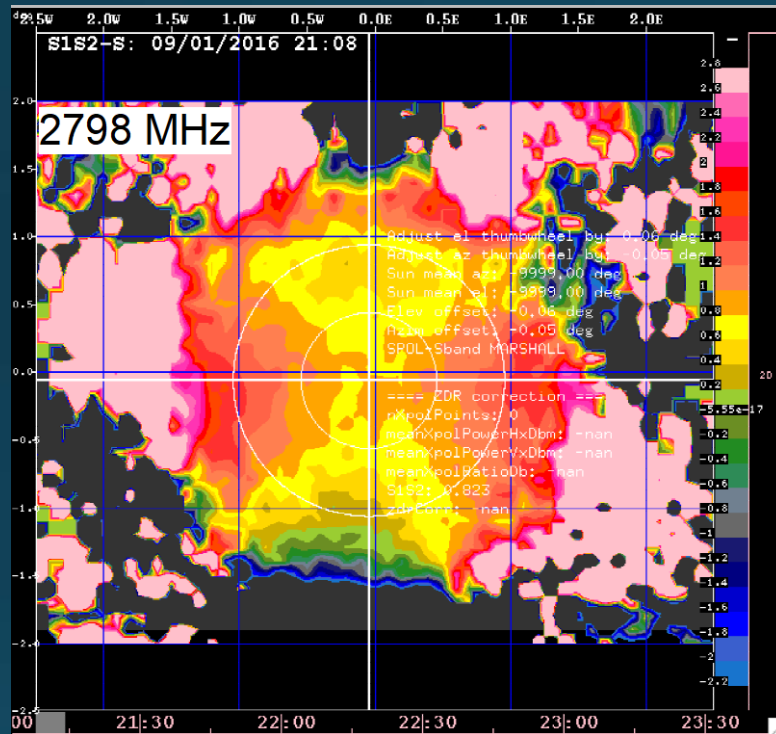


A change of 2 MHz causes a diff. gain change of 0.25dB!

Solar V/H power or Zdr Antenna Patterns



...continued Zdr Antenna Patterns



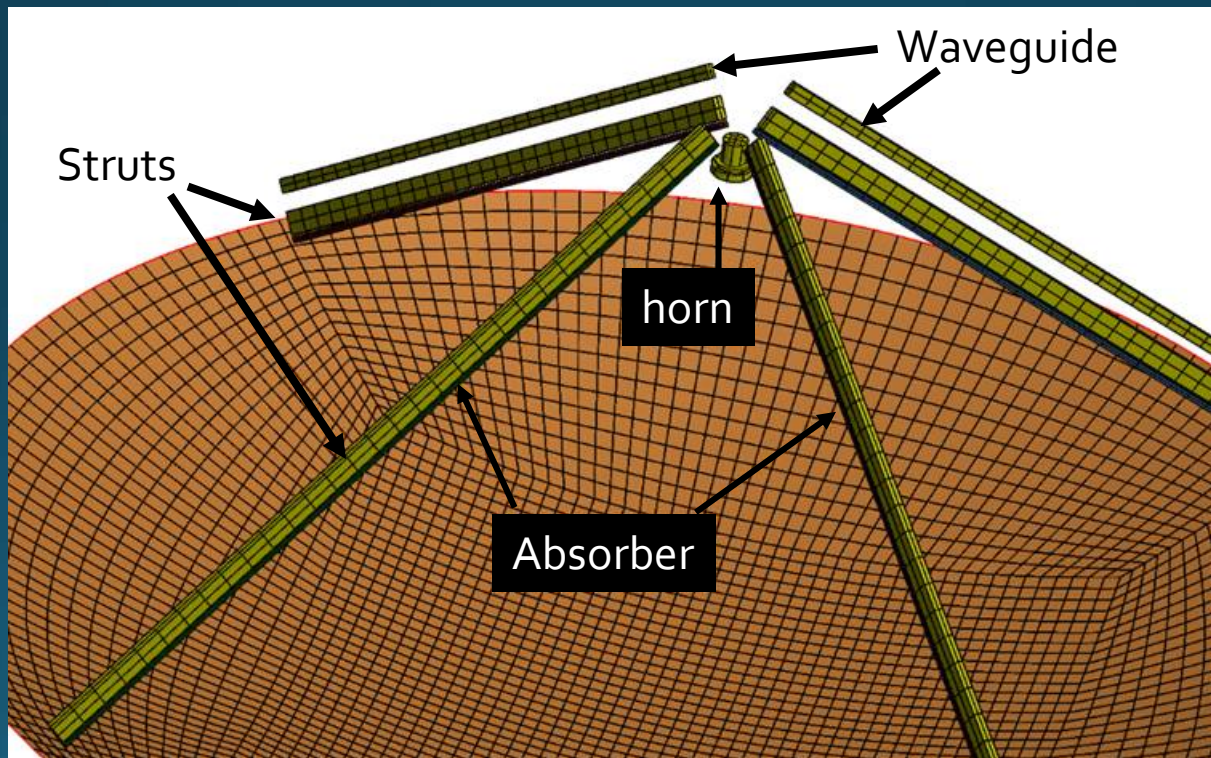
Dish Shape: Photogrammetry



- About 1400 optical patches on dish, struts and feedhorn.
- About 50 pictures around the edge of dish
- Fit a parabola
- RMS error across the dish: ~ 0.03 inch
- Exact dimensions of the feedhorn (CAD drawing)

Numerical Modeling of Antenna

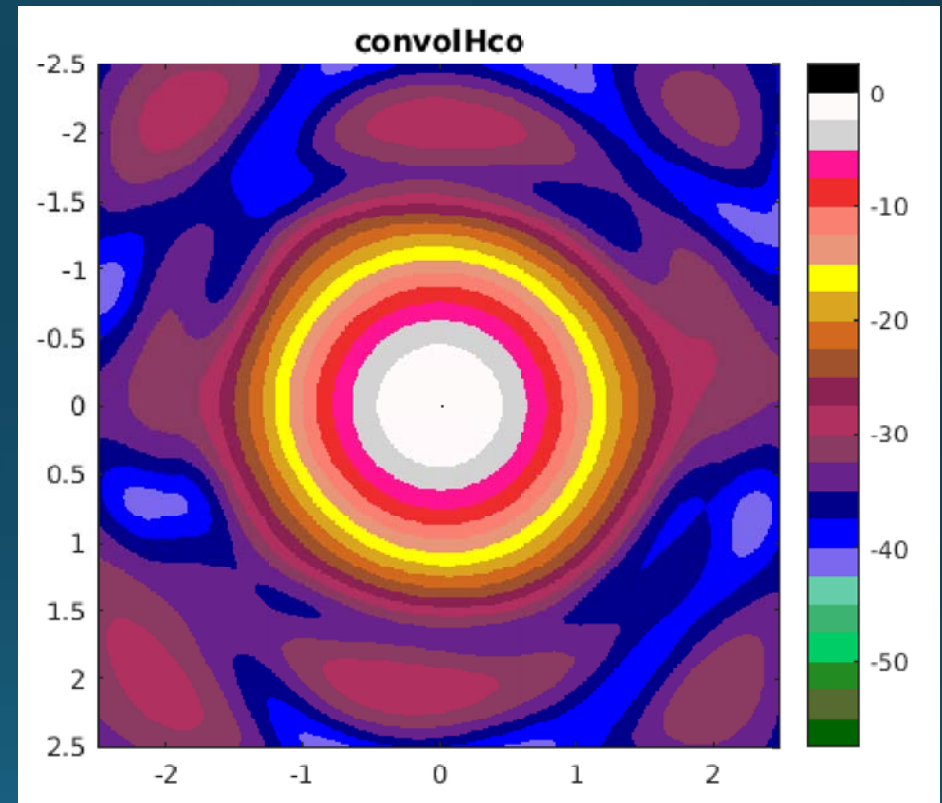
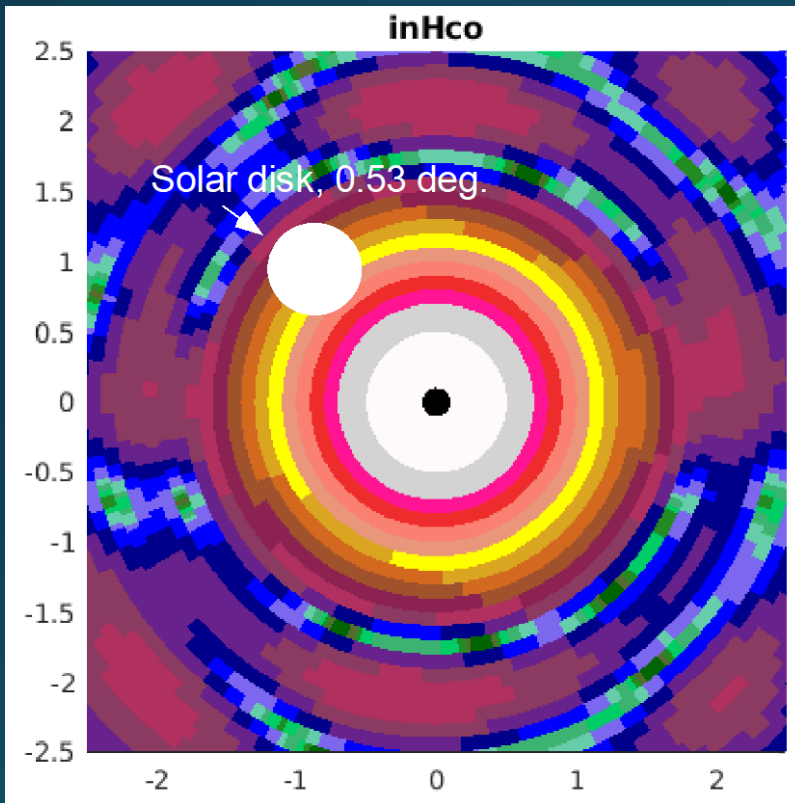
- Using GRASP (General Reflector Antenna Software Package) by TICRA of Denmark with the Method of Moments. This is an exact full wave method, which takes into account all mutual coupling, blockage and near-field effects.
- Exact dish shape
- Simulated feed horn patterns (from the horn CAD drawing)
- **COMPLEX COPOLAR AND CROSS-POLAR ANTENNA PATTERNS**



4 Cases Model

1. Full model
2. Without waveguide
3. Without absorber
4. Move feed horn phase center 3mm closer to dish

Convolve the Modeled Antenna Patterns with Solar Disk



Calculating Zdr from Model Data

$$Z_{DR} = \frac{\int |f_{HH}^2 + f_{HV}^2| d\Omega}{\int |f_{VH}^2 + f_{VV}^2| d\Omega}$$

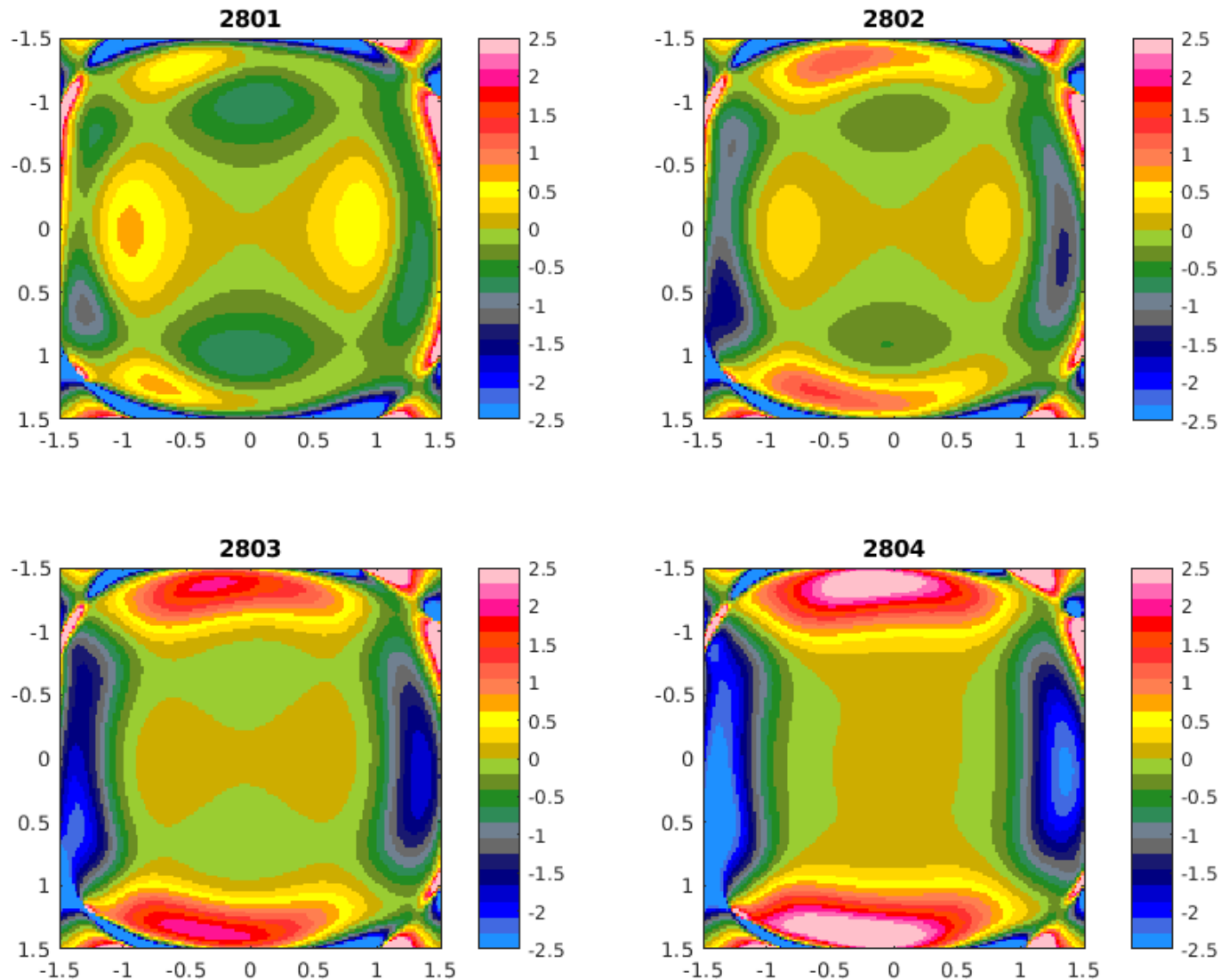
Complex antenna patterns!!

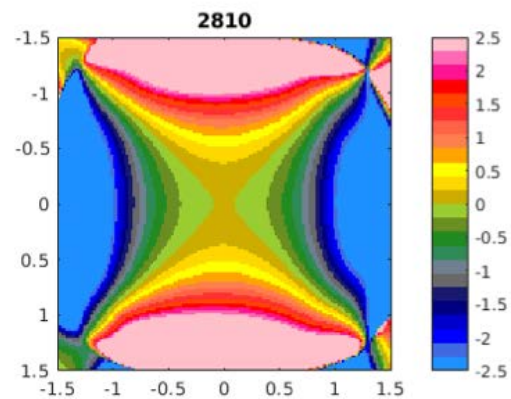
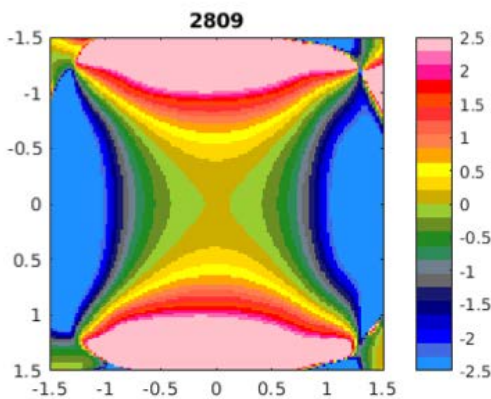
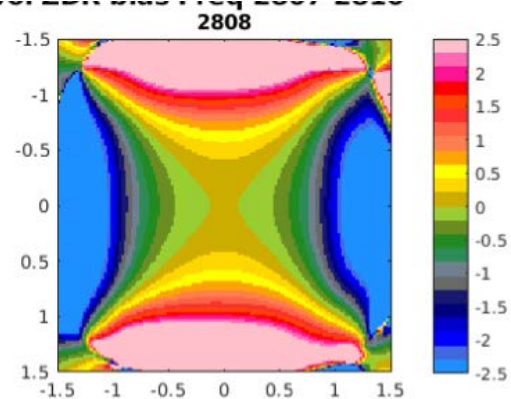
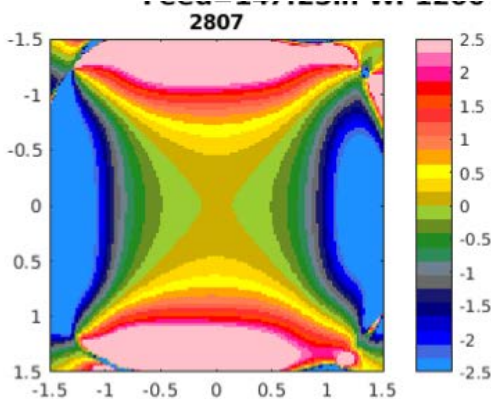
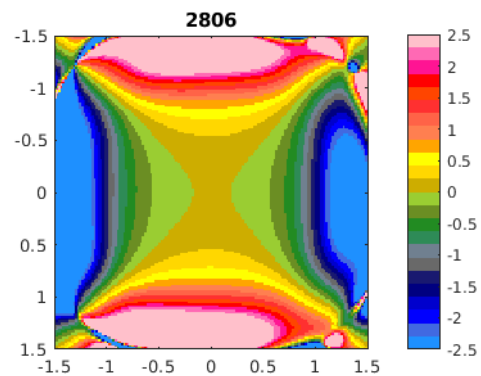
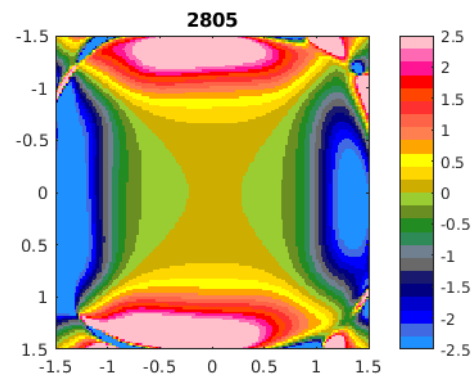
Chandrasekar and Keeler 1993

Modeled Zdr Antenna Patterns

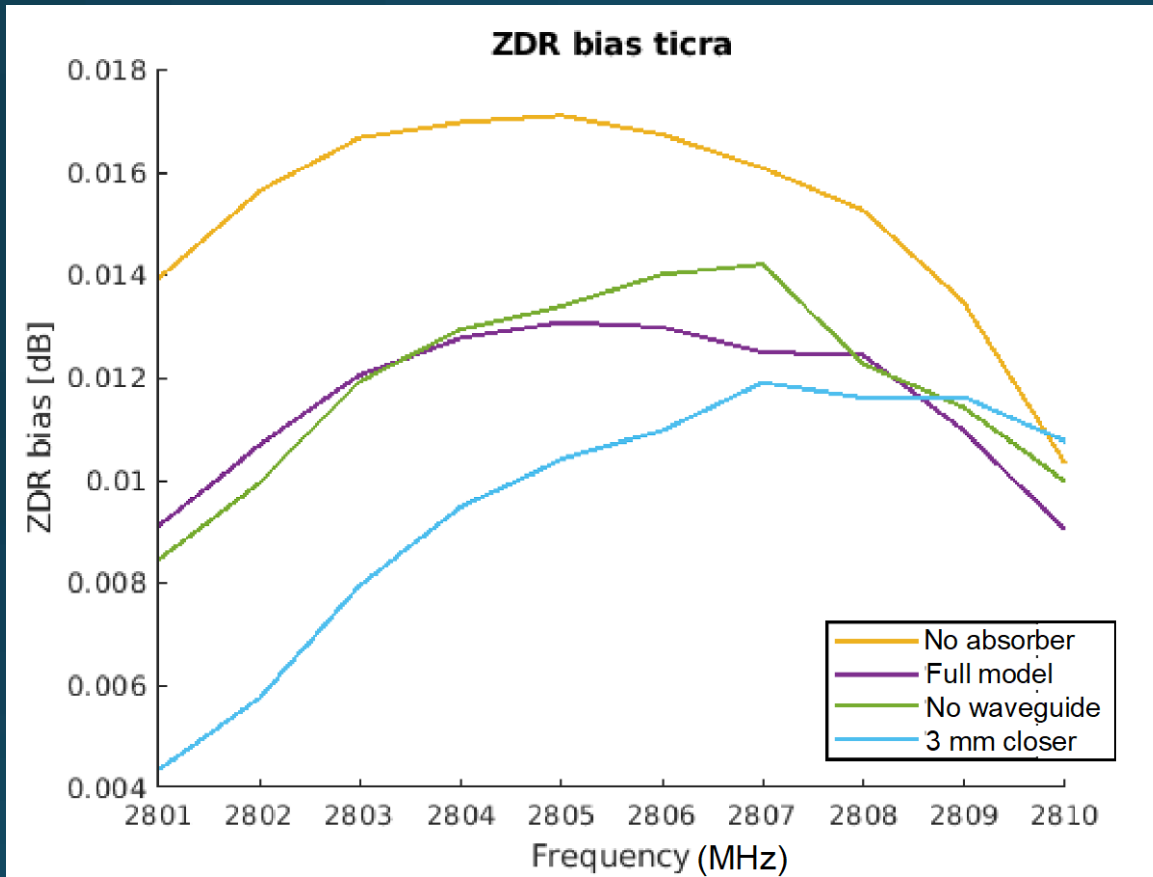
(convolved with solar disk)

Feed=147.25in WP1200 convol ZDR bias Freq 2801-2806

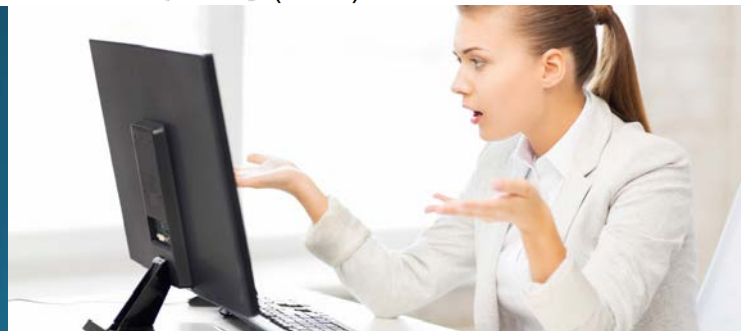




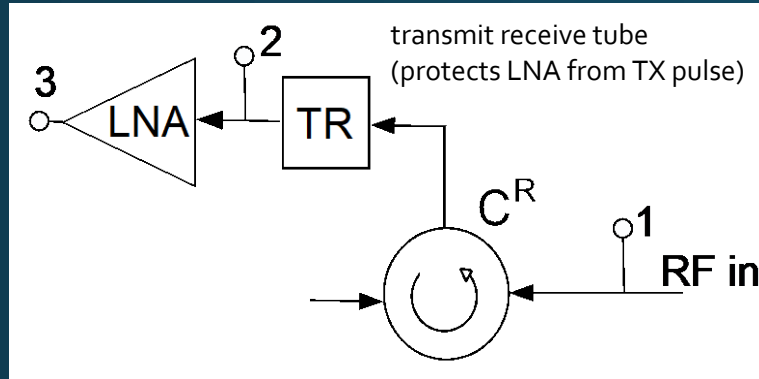
Integrated Zdr Bias



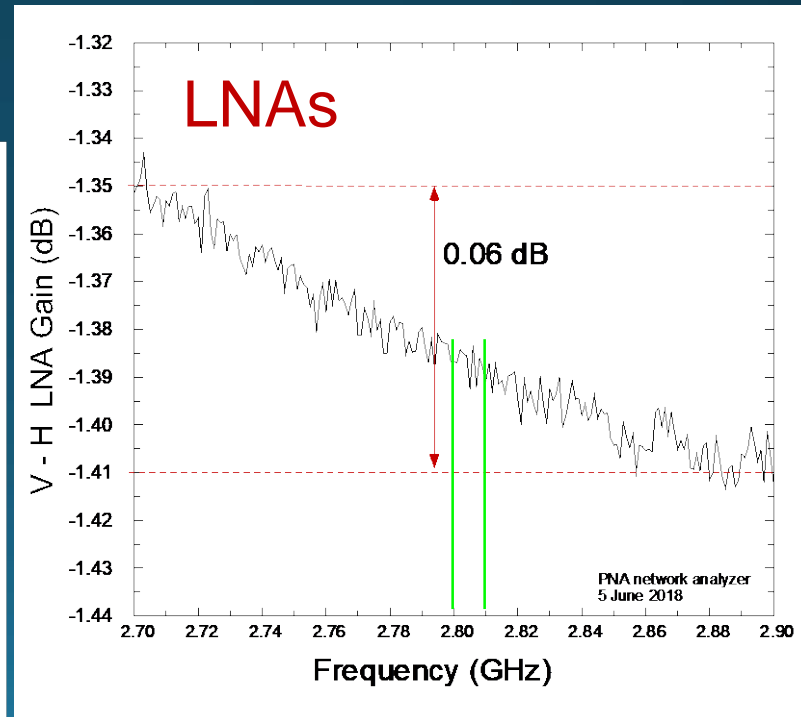
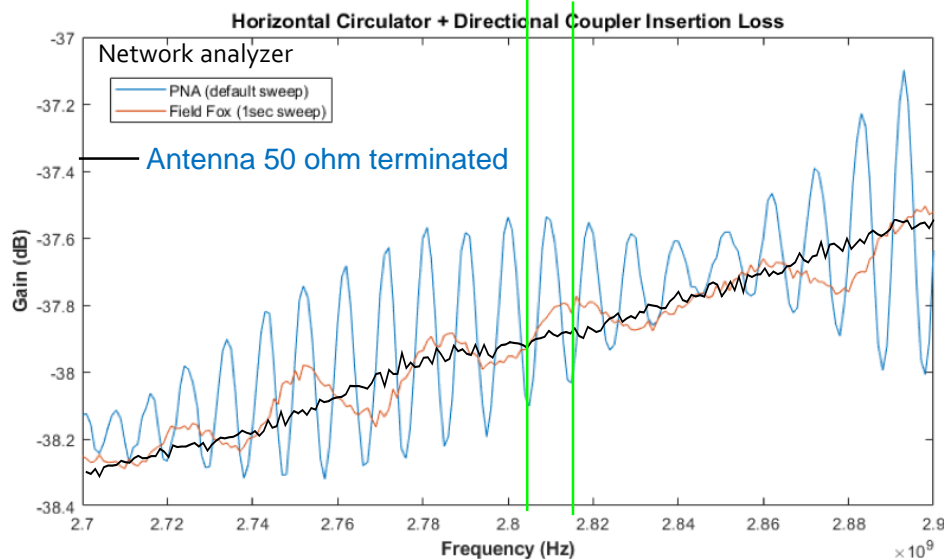
But Zdr bias
varies very
little!!



Differential Gain of RF Section



$$S_1 S_2 = \frac{(W_V G_V^A C_V^R LNA_V)^2}{(W_H G_H^A C_H^R LNA_H)^2}$$

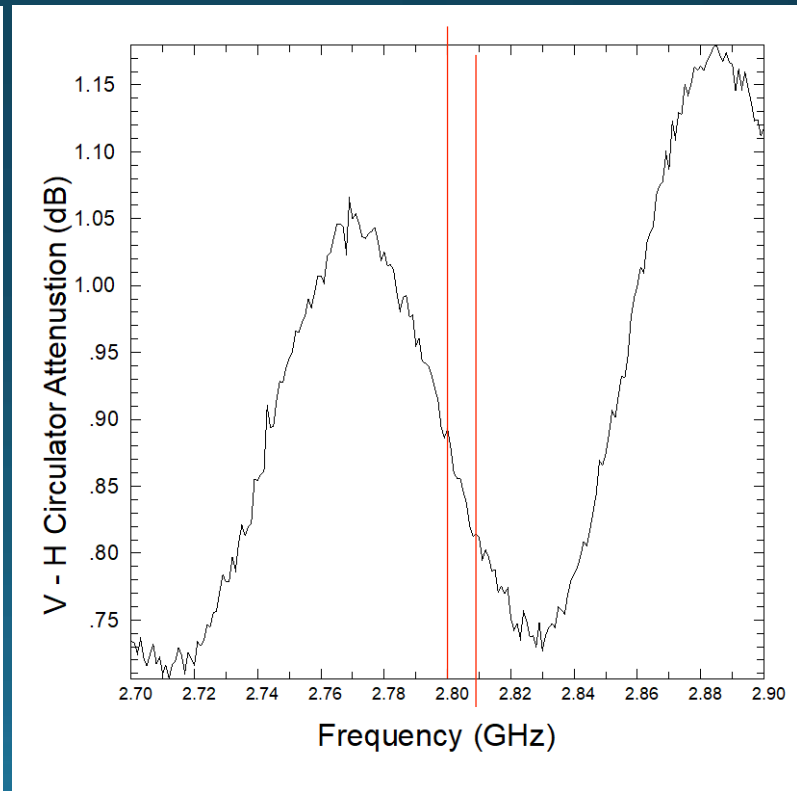
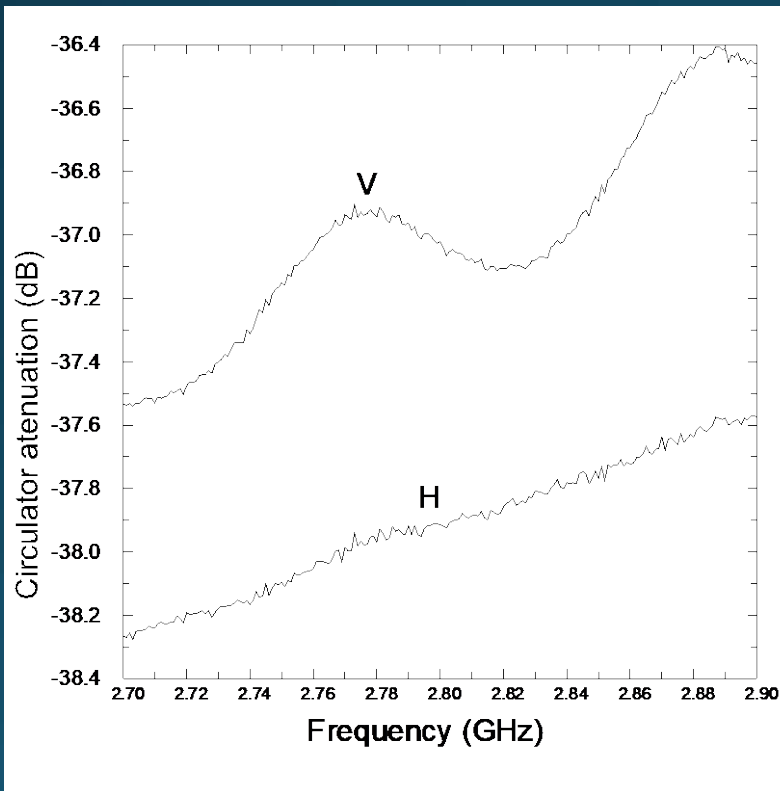


Likely that the RF diff. gain is cause the seen S1S2 frequency variation.

Circulator Attenuation

Wave guide to antenna terminated (50 ohms)

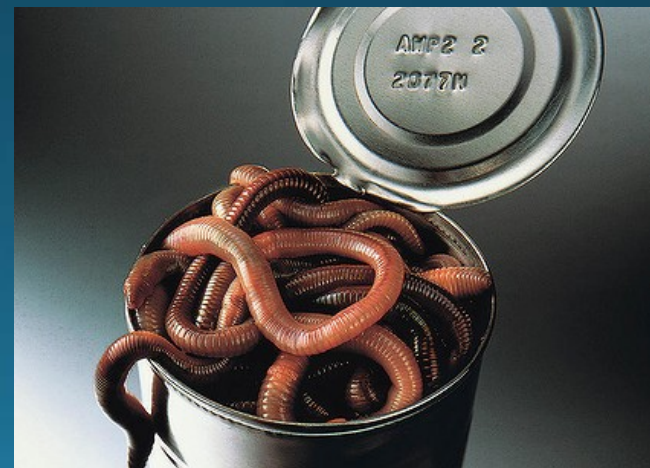
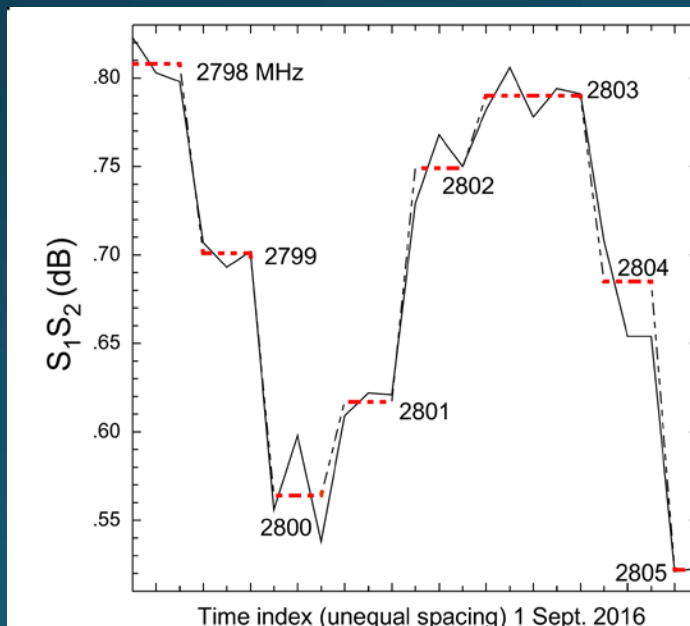
V-H Difference

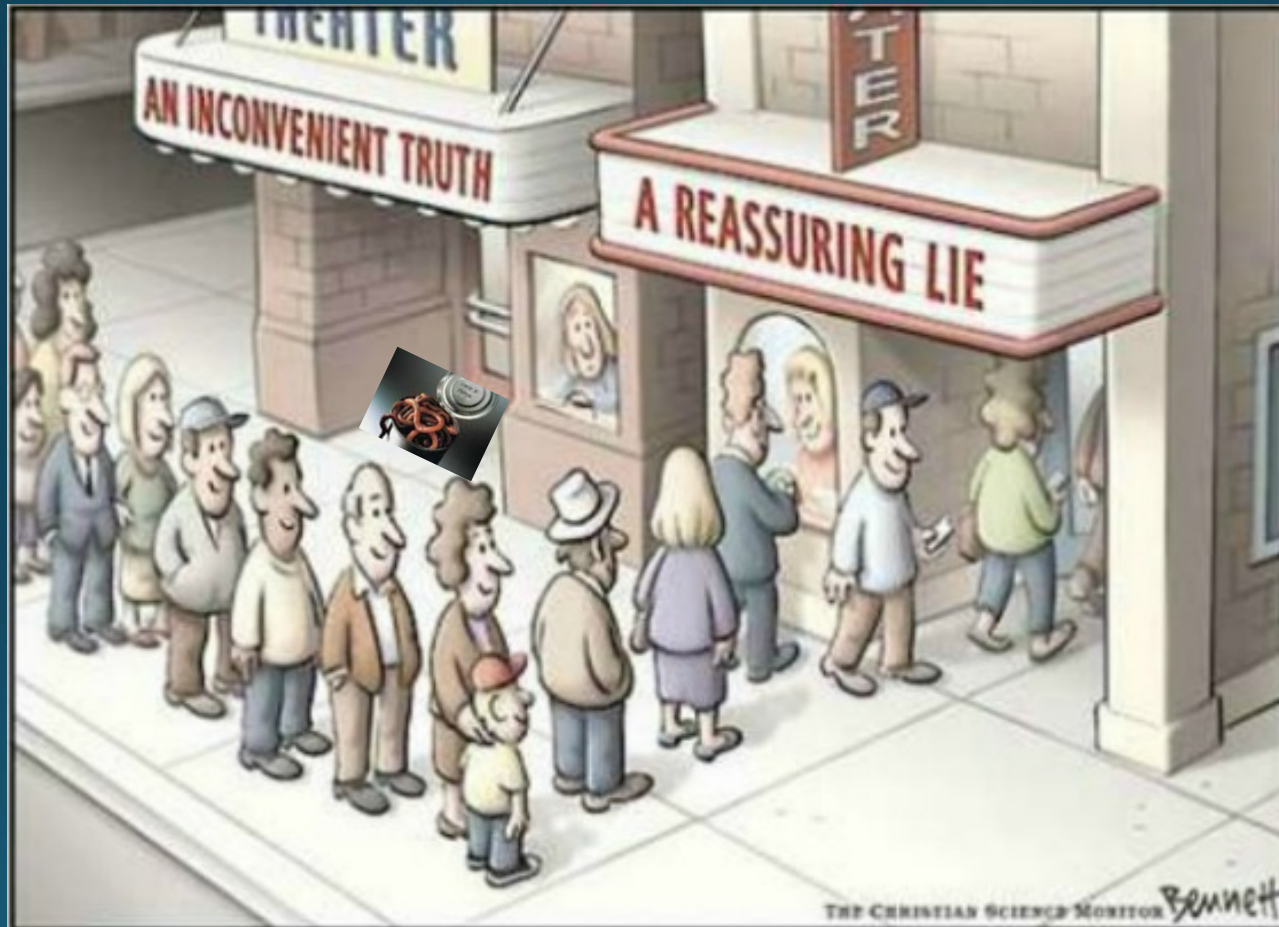


Antenna Solar Diff Gain S_1S_2

Conclusion ????

- Good question
- LNAs aren't the source of differential gain change
- The circulators appears the likely source
- The measurements of the circulator with and with out antenna termination are very different.
- So antenna impedance is a function of frequency so that the gain is affected





ICPR Patterns

Integrated Cross-Polarization Ratio

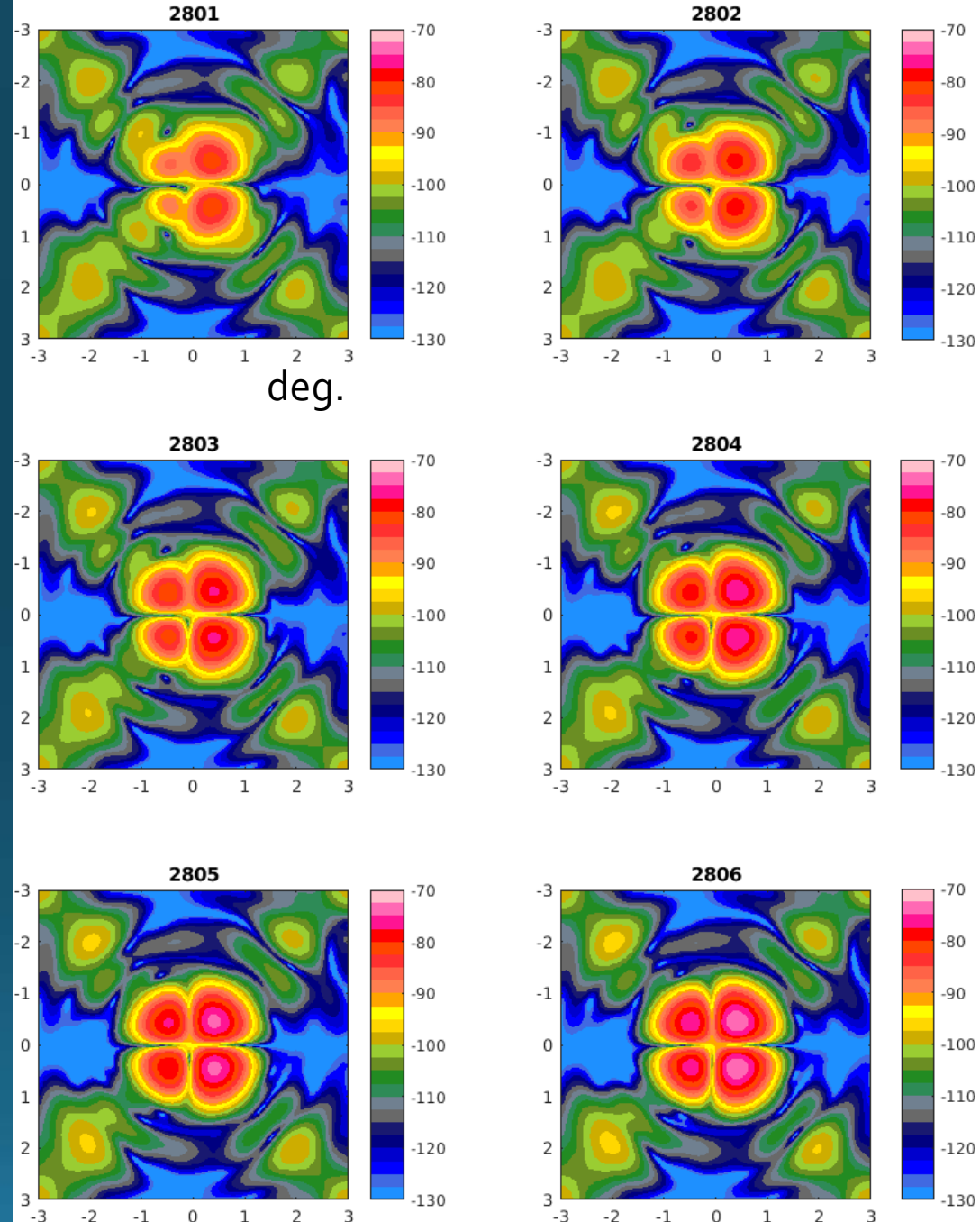
A measure of inter-channel isolation or polarization purity

$$\text{ICPR} = \frac{\int |f_{HH} f_{VH} + f_{HV} f_{VV}|^2 d\Omega}{\int |f_{HH}^2 + f_{VV}^2| d\Omega}$$

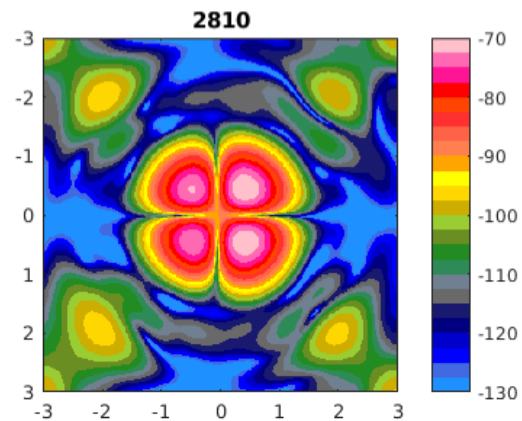
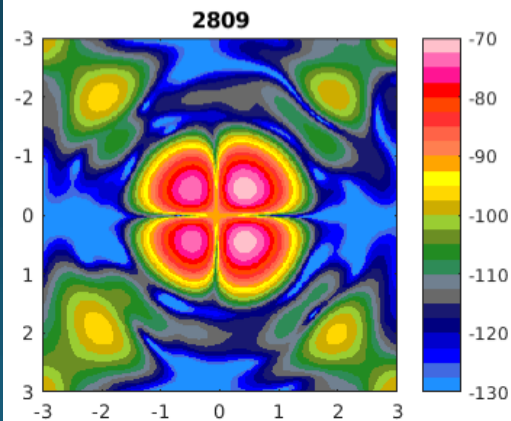
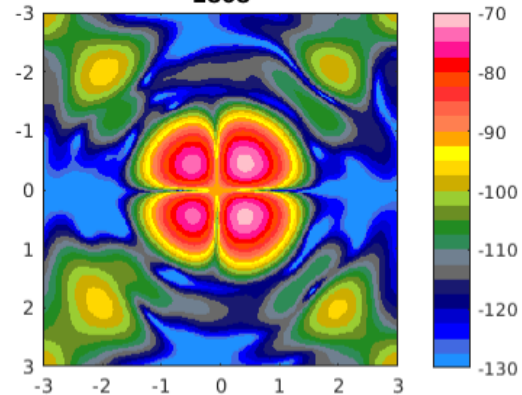
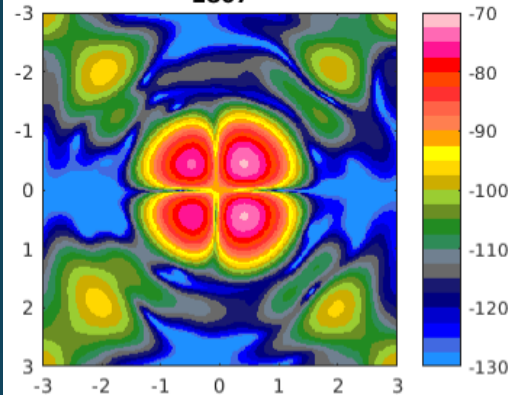
Wang and Chandrasekar, 2006,
IEEE Transactions on Geoscience
and Remote Sensing

“to limit Z_{dr} errors to +/-
0.2dB, -44dB isolation
needed.” (For SHV ops.)

Feed=147.25in WP1200 convol ICPR Freq 2801-2806



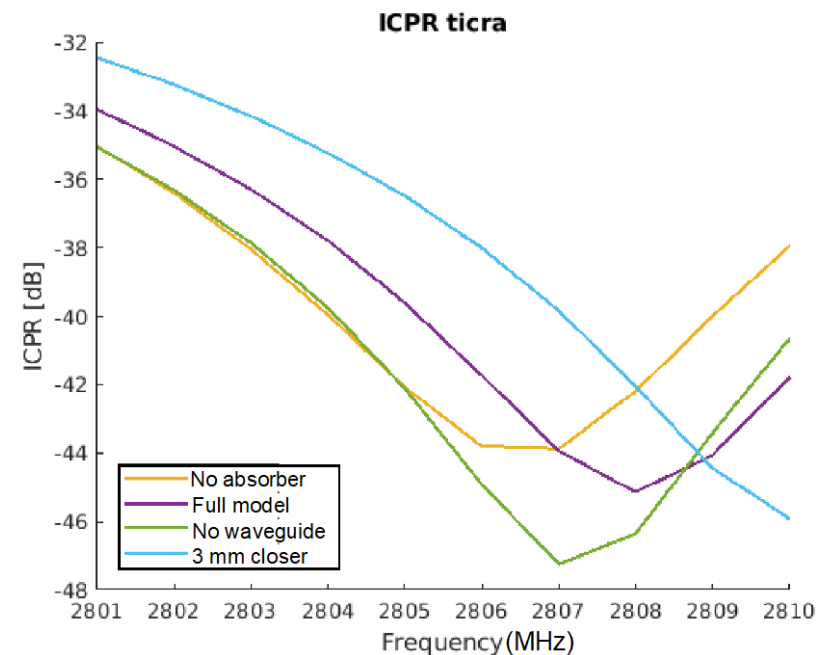
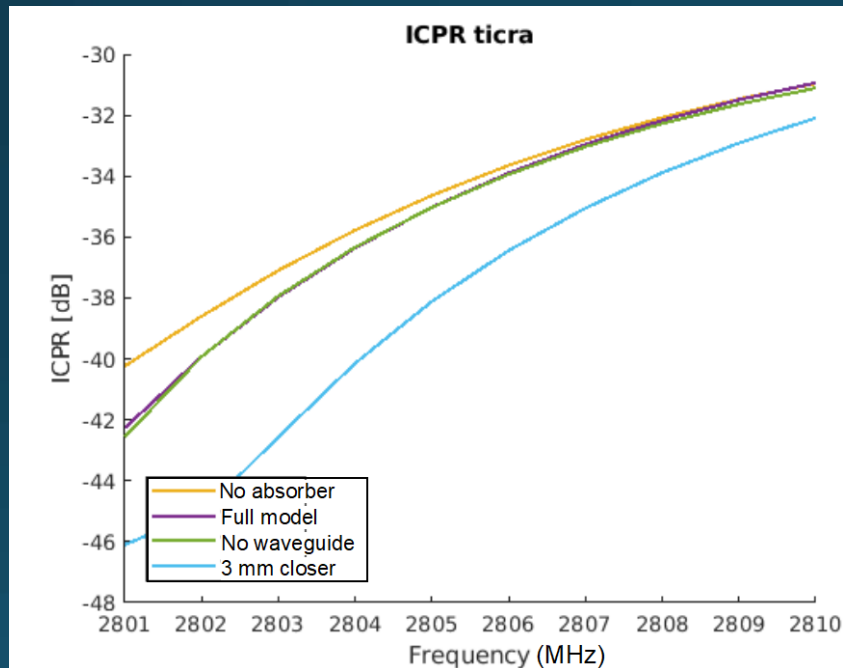
Feed=147.25in WP1200 convol ICPR Freq 2807-2810



Integrated ICPR

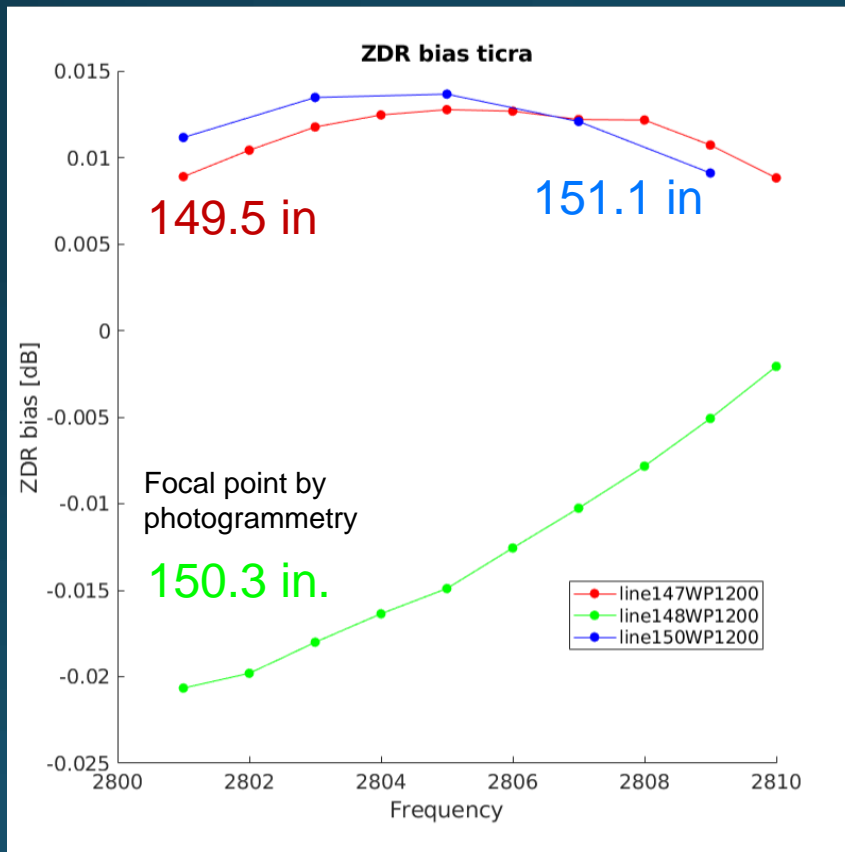
Phase center at 149.5 in

Phase center at 151.1 in

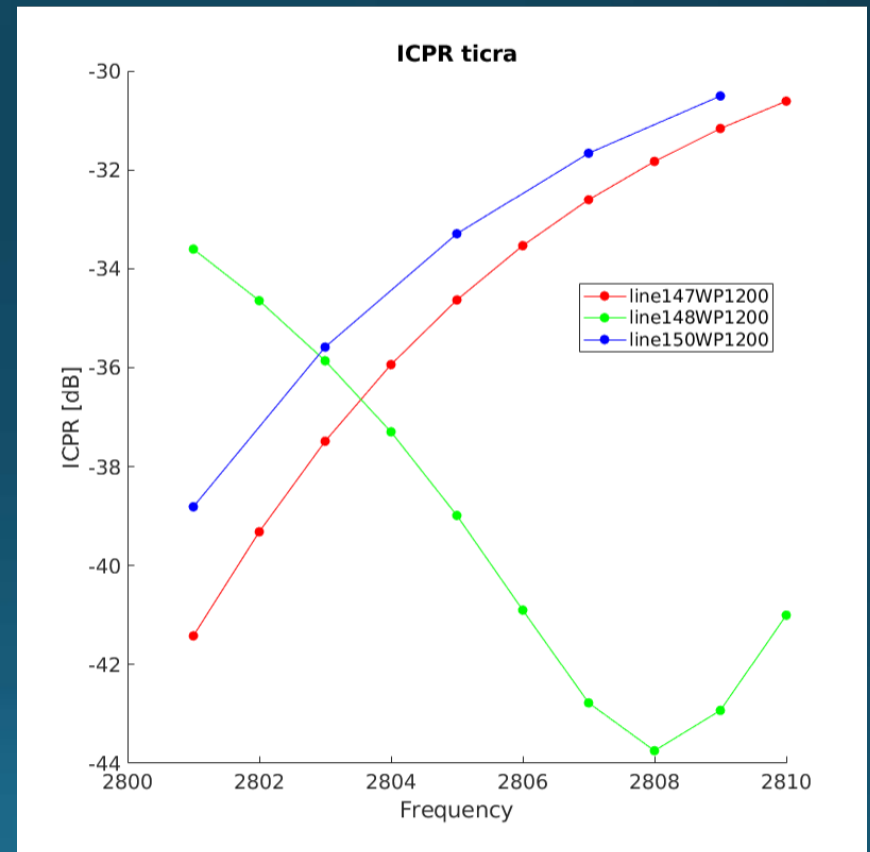


Full Model Comparison for 3 Phase Center Locations

Zdr Bias

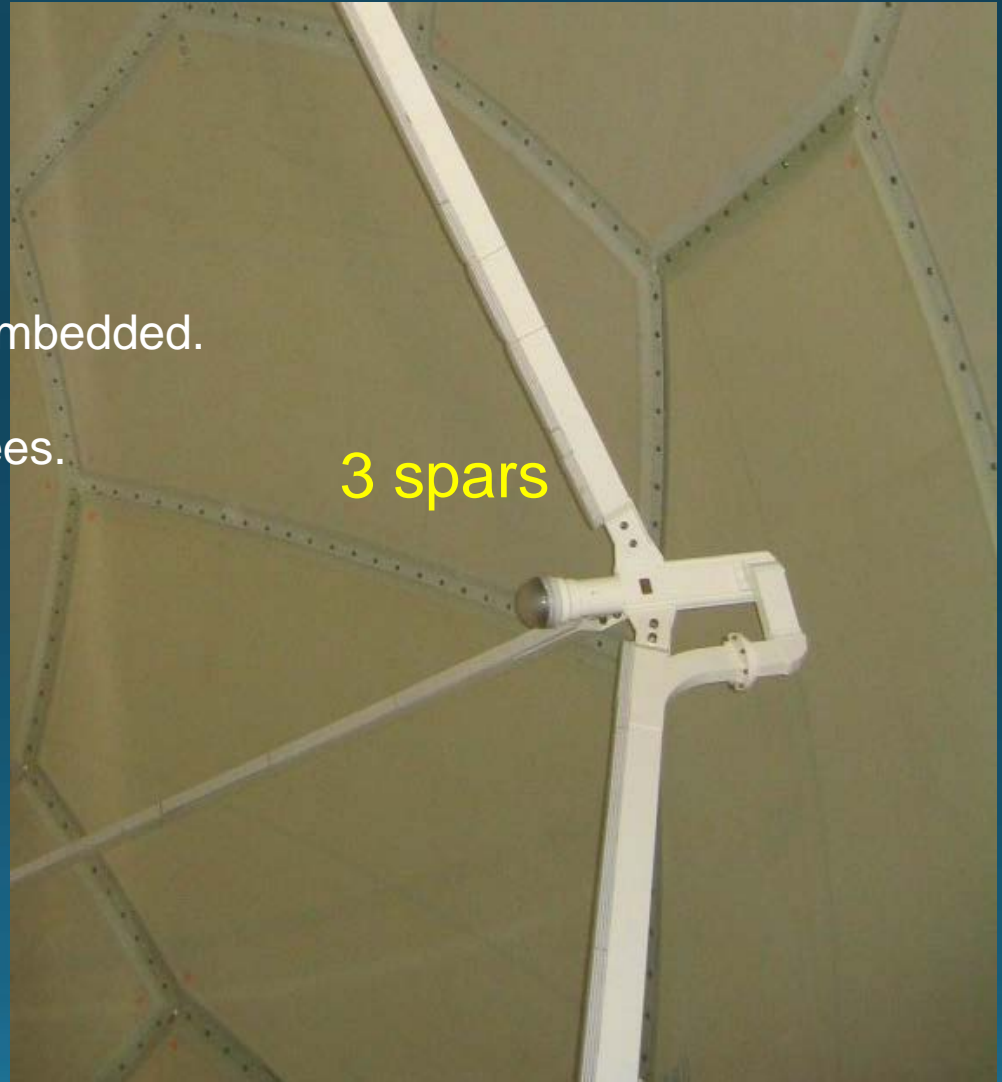


ICPR

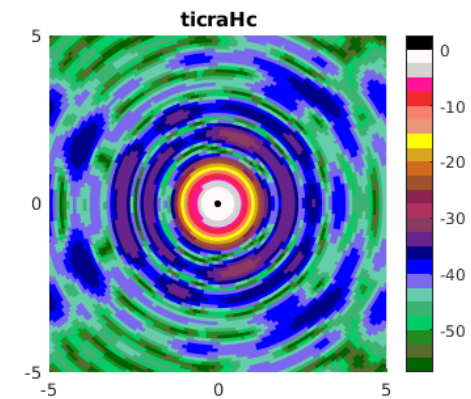


NEXRAD: Modeling the WSR-88DP

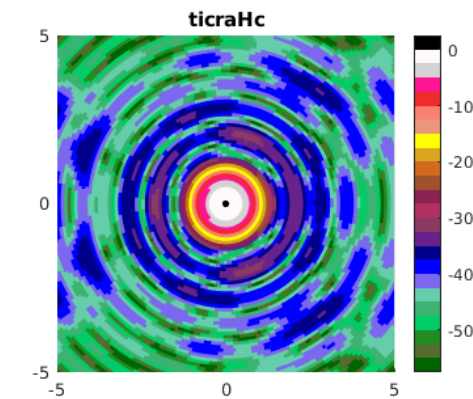
- Three spars with waveguide embedded.
- Absorber on spars.
- Spars at 0, 120 and 140 degrees.
- Cad drawing of feed horn.
- Did not model radome.



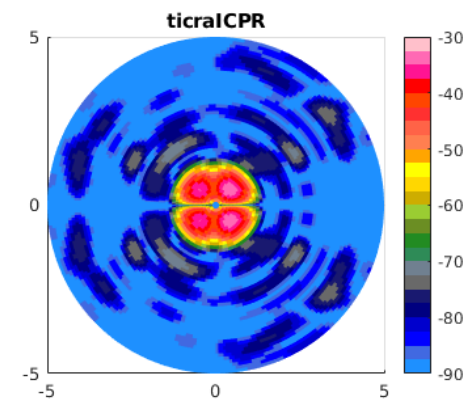
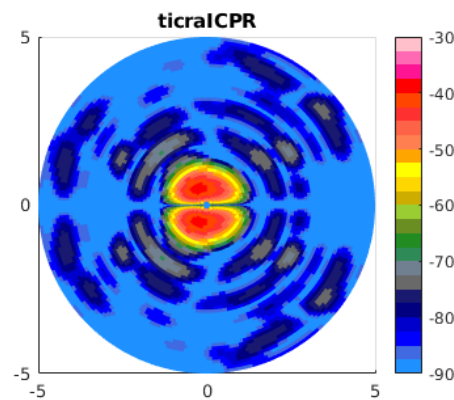
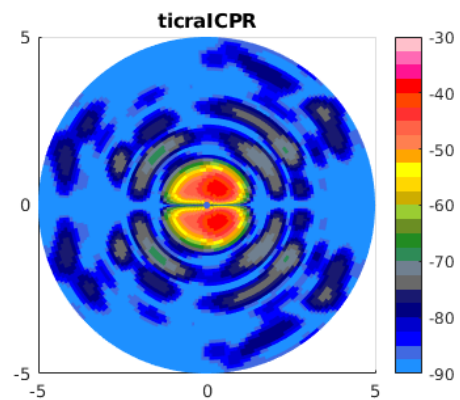
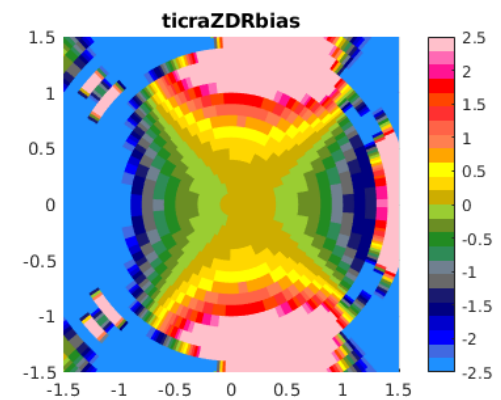
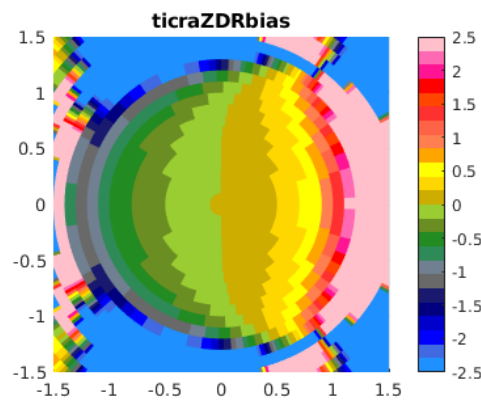
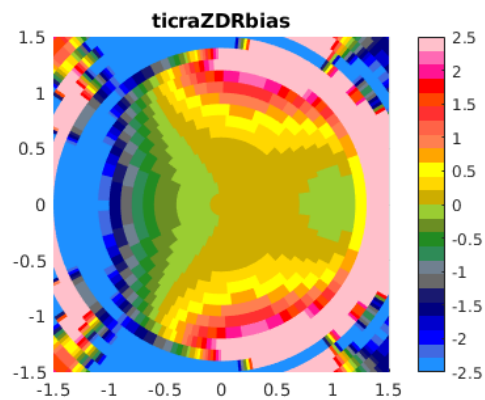
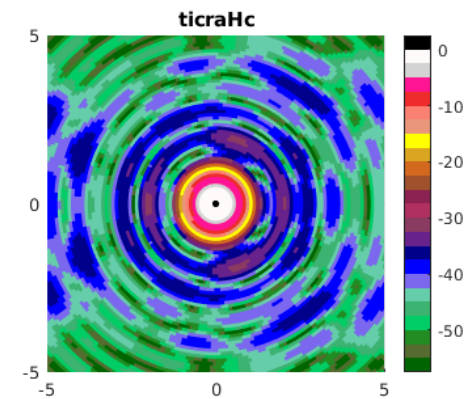
nexrad Freq=2700



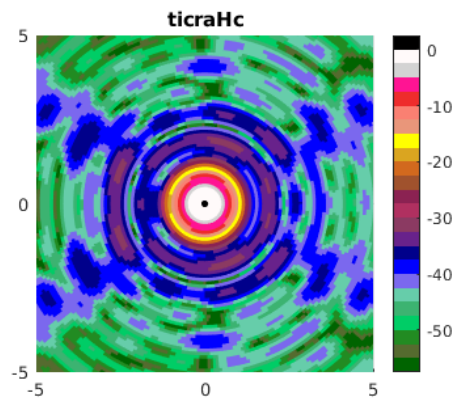
nexrad Freq=2705



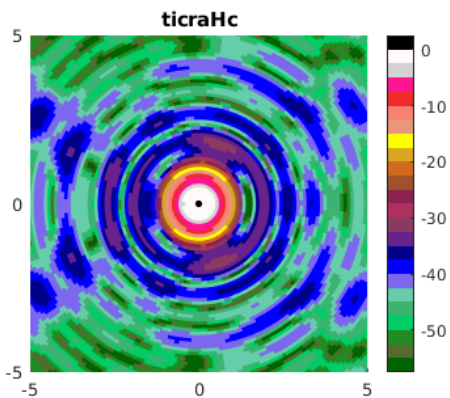
nexrad Freq=2800



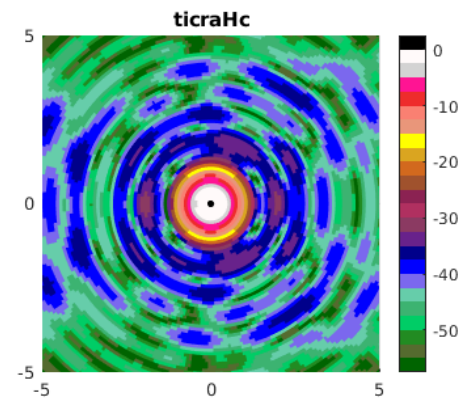
nexrad Freq=2880



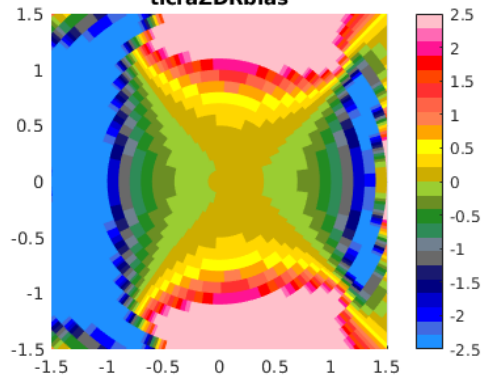
nexrad Freq=2890



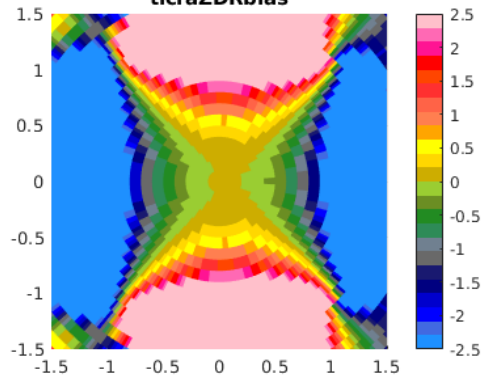
nexrad Freq=2900



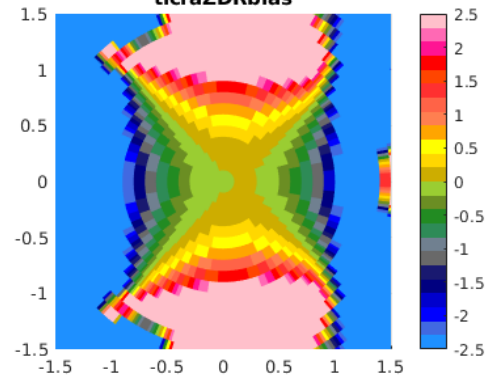
ticraZDRbias



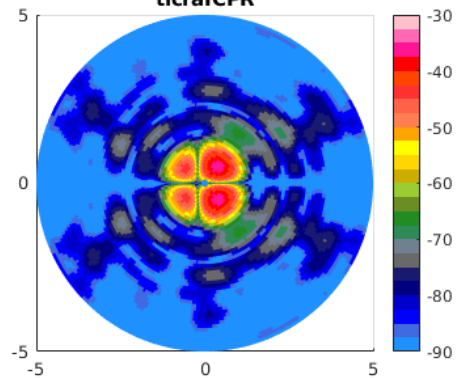
ticraZDRbias



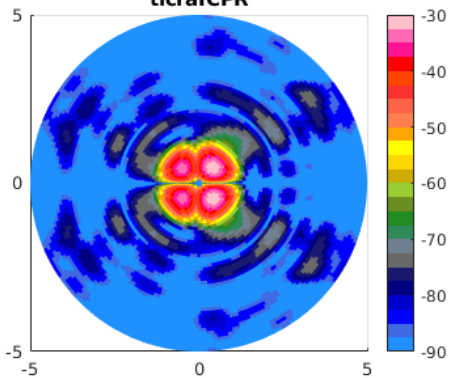
ticraZDRbias



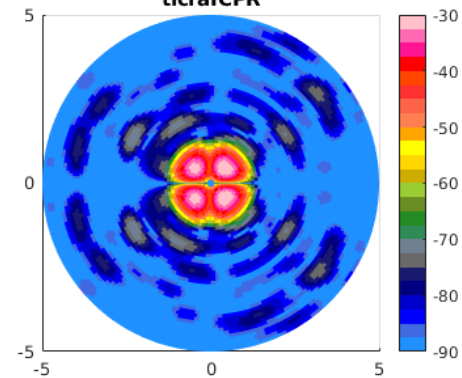
ticraICPR



ticraICPR



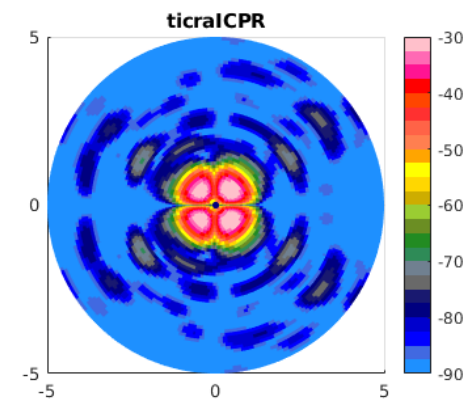
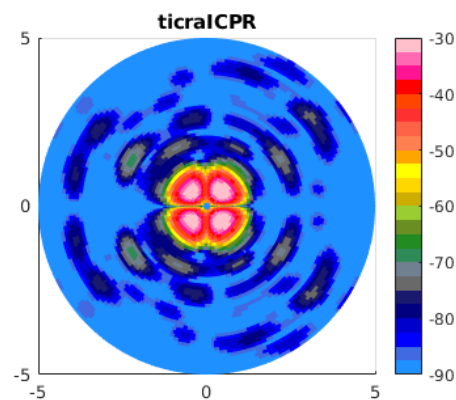
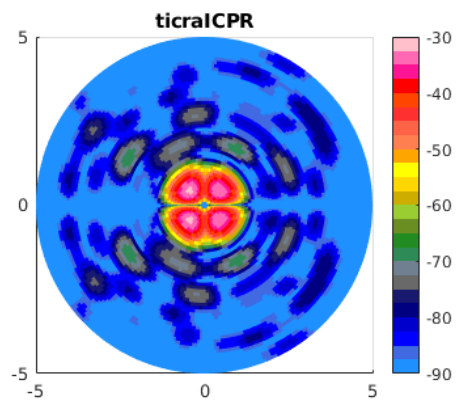
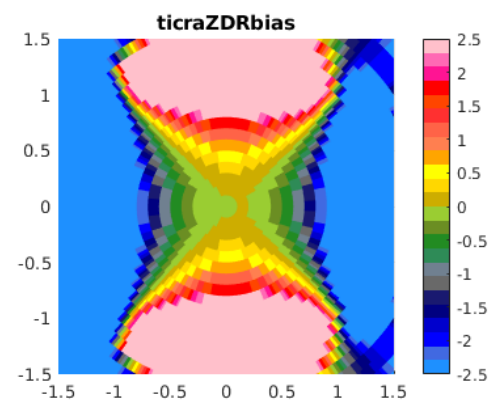
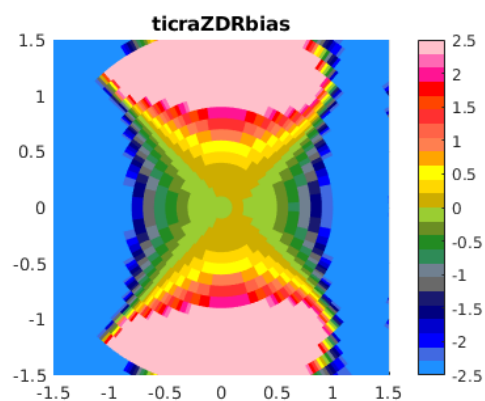
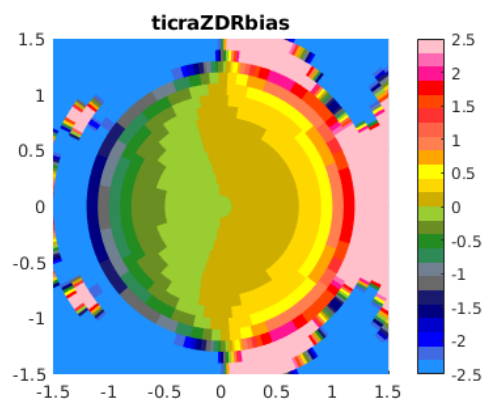
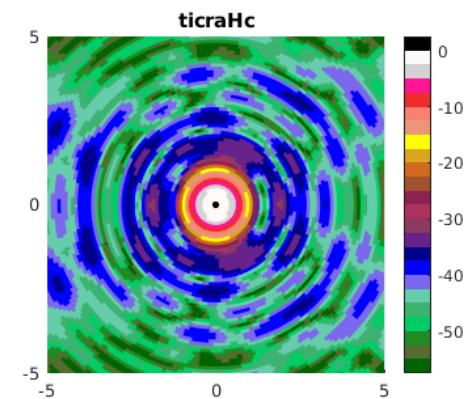
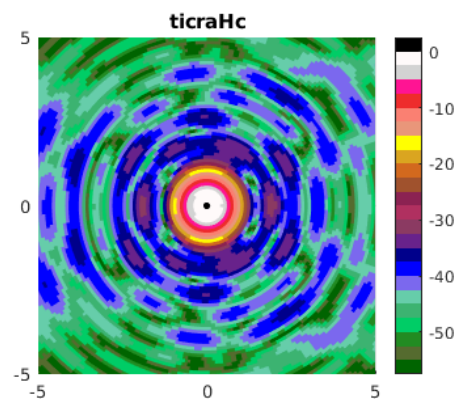
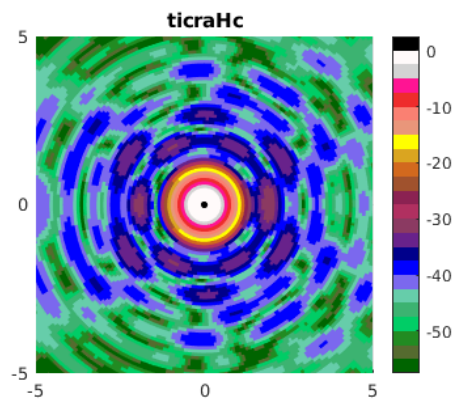
ticraICPR



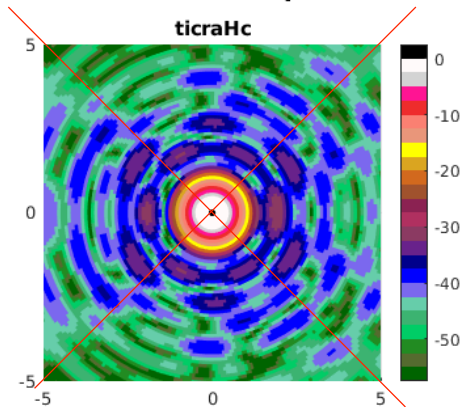
nexrad Freq=2910

nexrad Freq=2950

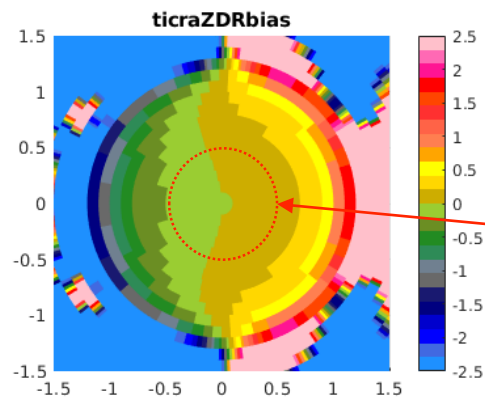
nexrad Freq=2995



nexrad Freq=2910



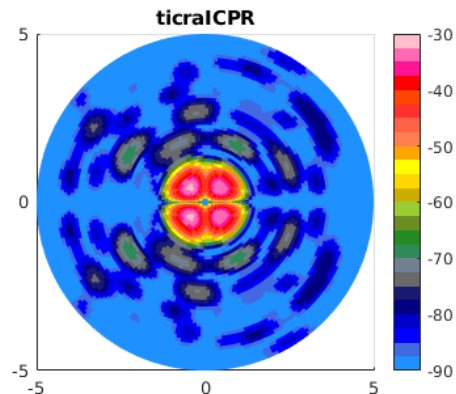
Side lobes are not highest along ± 45 degree cuts



Zdr bias pattern can have gradients across it.
0.2 dB color steps.



1 degree solid angle



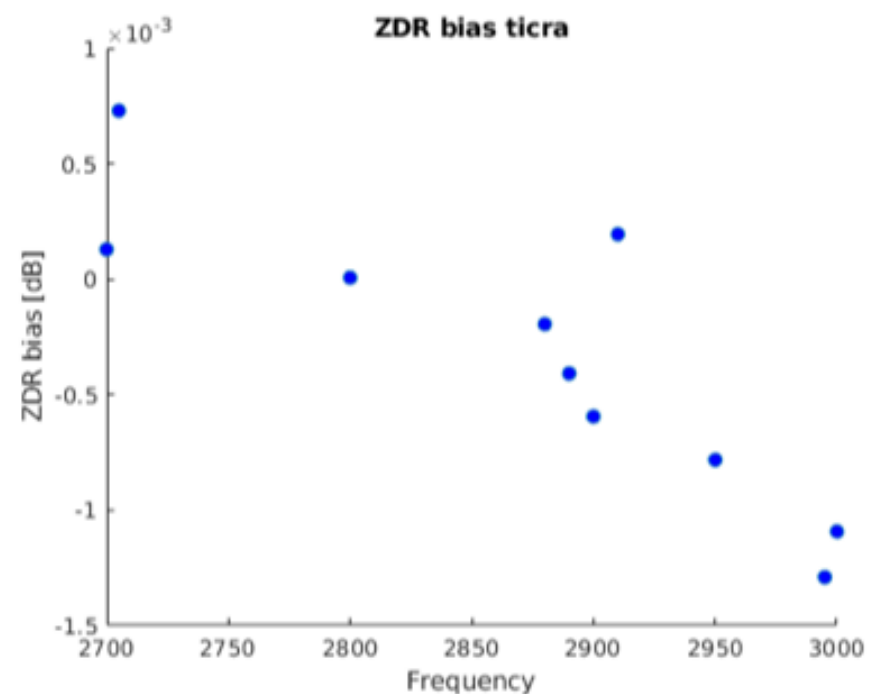
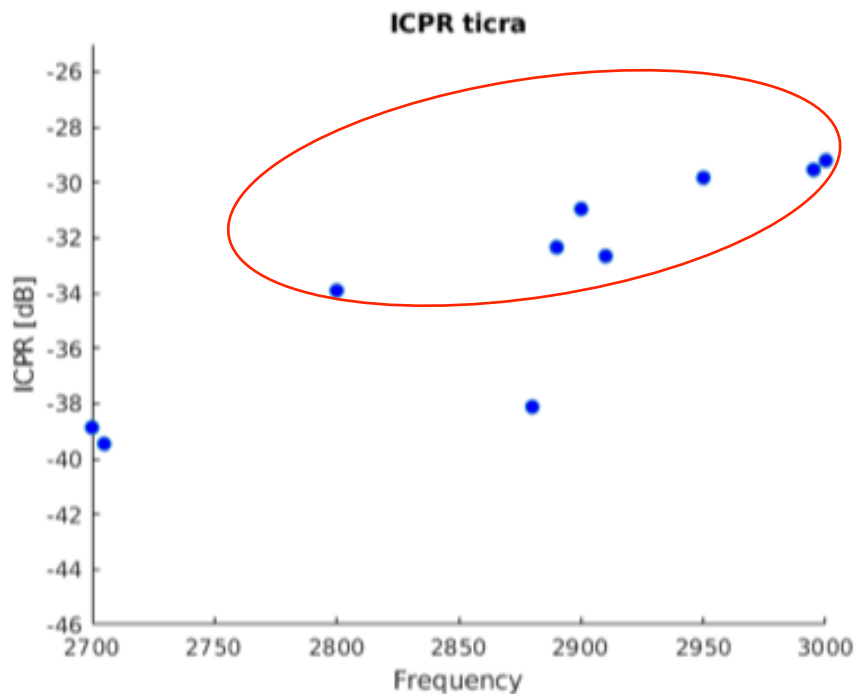
ICPR pattern looks similar to S-Pol $\frac{4}{3}$ spar model data



WSR-88DP: Zdr Bias and ICPR

These higher values indicate cross coupling could be a problem for higher phidp accumulations

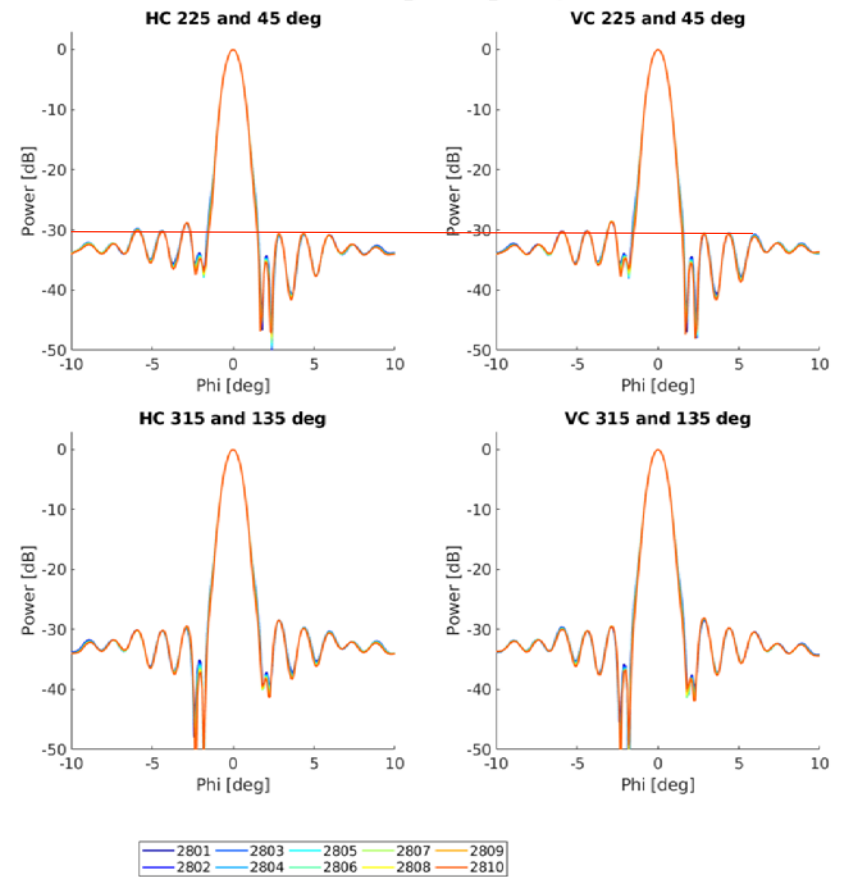
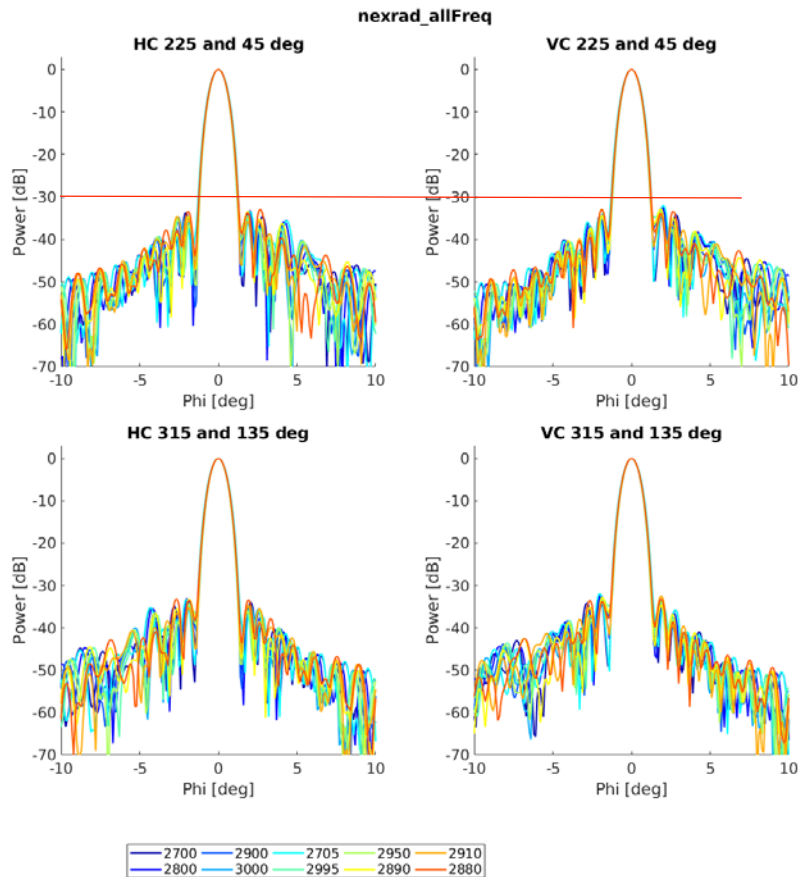
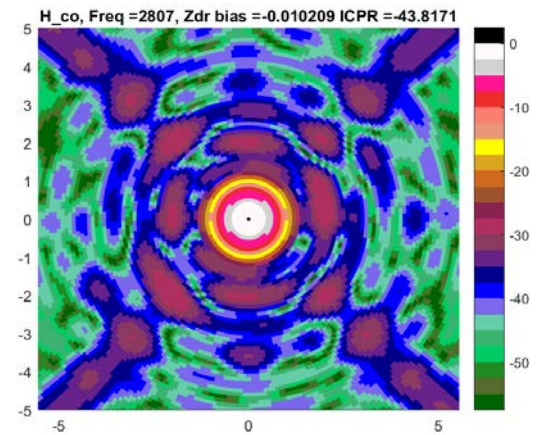
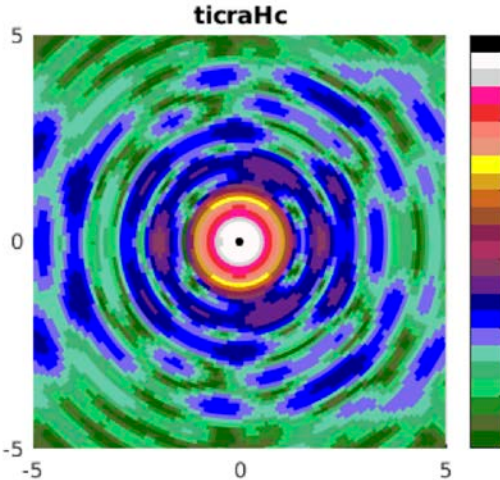
Zdr offset is a function of frequency but will be corrected by Zdr calibrations



The +/- 45 Degree Antenna Pattern Cuts

WSR-88DP, 3 spar

S-Pol, 4 spar



Observations

- S_1S_2 (Zdr) antenna pattern SHAPE changes for both temperature and frequency changes
- **GRASP MODEL:** predicts Zdr shape changes but, S_1S_2 differential gain is not predicted
 - *RF component's differential gain causes the observed frequency dependent dif. gain.*
- **EXPERIMENTAL:** S_1S_2 integrated does change substantially for changes in temperature: $\sim 0.01\text{dB/C}$
- Expansion/contraction of the entire antenna structure causes both Zdr antenna pattern shape as well as Zdr bias to change.
- **ICPR** is a complicated function of frequency and antenna topology

Hubbert, J. C., 2017: Differential reflectivity calibration and antenna temperature. *J. Atmos. Oceanic Technol.*, <https://doi.org/10.1175/JTECH-D-16-0218.1>

ICPR: Cross Coupling

- Very sensitive function of frequency
- Zdr bias for simultaneous H and V transmit radars is a function of this cross coupling (channel isolation)
- To keep Zdr bias to within 0.2dB, isolation should be -44dB (Wang and Chandrasekar 2006)
- ICPR is a sensitive function of phase center location

- WP1100: Geometry including 4 struts and 2 waveguides
- WP1200: Geometry including 4 struts with absorbers and 2 waveguides
- WP1300: Geometry including 4 struts with absorbers
- WP1400: Geometry including 4 struts with absorbers and 2 waveguides and feed moved 3 mm closer to the reflector